

Shock-turbulence interaction: an exhaustively classifying linearized approach *

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■ Main topics: hyperbolic systems of conservation laws, gas dynamics. ■ The context of the considered interaction assumes a *minimal* nonlinearity – in the form of a nonlinear subconscious. Consequently the interaction solution is essentially constructed as an admissible solution. The present analysis has essentially two objectives: (a) finding an *explicit optimal form* for the interaction solution, and (b) offering an *exhaustively classifying characterization* of this mentioned solution. ■ Realizing the objective (a) is connected with: (a₁) considering a *singular limit* of the interaction solution, (a₂) considering a *hierarchy of (natural) partitions* of the singular limit, (a₃) inserting some (natural) *gasdynamic factorizations* at a certain level [see sections 4.3, 4.5 and 4.7] of the mentioned hierarchy and (a₄) noticing a *compatibility* of these factorizations (indicating a gasdynamic *inner coherence*), (a₅) *predicting some exact details* of the interaction solution, (a₆) indicating some parasite singularities [= strictly depending on the method] to be compensated [= pseudosingularities], (a₇) *re-weighting* the singular limit of the interaction solution. ■ Realizing the objective (b) is connected with finding some *Lorentz arguments of criticality*. ■ The interaction solution appears essentially to (exhaustively) include a *subcritical* and respectively a *supercritical* contribution distinguished by differences of a “relativistic” nature. Precisely: in the singular limit of the interaction solution [cf. (a₁)] the emergent sound is *singular* in the subcritical contribution and it is *regular* in the supercritical contribution (see Figure 3). It can be shown that this “relativistic” discontinuity in the nature of the emergent sound, corresponding to the singular limit of the interaction solution appears to be dissembled (hidden) in the re-weighted interaction solution [mentioned in (a₇)].

1. THE MAIN RESULTS

The aim of this paper is to consider, in a linearized context, the interaction between two gasdynamic objects: a *turbulence model* and, respectively, a *planar shock discontinuity*. The turbulence, regarded as a perturbation, is modelled by a nonstatistical /noncorrelative superposition of some compressible finite core (or point core) planar vortices. The *linearized* context implies the taking into consideration of a linear problem with a *nonlinear subconscious*; the resultant perturbation is regarded as a solution (“interaction solution”) of such a *linearized* problem. The turbulence – planar shock interaction is associated with a class of interaction elements. An interaction element models the interaction between a planar shock and a *single* incident vortex corresponding to a certain inclination of the vortex axis with respect to the shock.

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Modelling the incident turbulence by a superposition of compressible planar vortices appears to correspond to a *first level* of decomposition; next, in order to proceed, each incident vortex is decomposed (by a Fourier representation) into planar monochromatic waves – a *second level* of decomposition; finally, each incident planar monochromatic wave is Snell passed through the shock discontinuity. The composition of the two mentioned levels leads to a Fourier–Snell representation of the interaction solution (cf. §§3–5). The main point of the analysis in §§3–5 is that the result of the passage through the shock can again be presented by two levels of *recombination* so that each incident level of decomposition has a correspondent in the emergent solution.

A Fourier–Snell representation of the linearized interaction between a planar shock discontinuity and a planar compressible finite-core vortex the axis of which is *parallel* to the shock has been considered first time by Ribner (1959) in a theoretical attempt consecutive to a pioneering and most suggestive experimental approach of Hollingworth and Richards (1956) concerning the mentioned interaction. An ample and significant series of theoretical and experimental developments has followed the two mentioned works [see Ribner (1985), for a thorough review].

The results of the present paper follow from an analysis initiated in Dinu [2] and considered in a thorough detail in Dinu [3]. This analysis would imply: (i) to notice a *gasdynamic factorization* of the vorticity–shock interaction and to make use of this factorization to give an **explicit, closed form** to Ribner’s representation; (ii) to identify a sequence of *other five gasdynamic factorizations* in the explicit form of the vortex–shock interaction solution [since a vortex represents a *structured* vorticity, the present factorizations appear to be induced by that mentioned in (i) by structuring] and to take into account the reality of a *factoring compatibility* of these factorizations (indicating an *inner coherence*) in order to select an **extensible** (to the case of the oblique interactions) structure of the mentioned explicit form ; an *optimal simplicity* is seen to be induced in the extensible structure by this factoring compatibility; (iii) to use the mentioned extensible structure in order to indicate an **exhaustively classifying, deterministic** and *explicit* characterization of Lighthill’s *statistic* and *implicit* approach concerning the turbulence – planar shock interaction. The resulting classification takes into account the importance of some *subcritical* or *supercritical* inclinations of the incident vortices with respect to the shock in the mentioned interaction.

A final (extended) version of the above mentioned analysis consists in replacing the *vorticity* incident perturbation by a *general gasdynamic* incident perturbation. This version extends particularly (cf. Dinu [4]) the paper Dragoş [8]. In fact it may be proven that the structure (i)–(iii) of the above mentioned interaction analysis *persists* in this final version.

The results presented in this paper correspond to a “*minimal*” nonlinearity [associated to the presence of a nonlinear subconscience]; still, they structure a *maximal* (exhaustive; explicit and oblique) classifying characterization of the turbulence–shock interaction.

The present analysis could be set in contrast with a lot of recent studies which allow (analytically or numerically) a *more complete* considering of the nonlinearity contribution yet in presence of the *minimal* case of a (strictly) parallel interaction; see for example Grove and Menikoff [9], Han and Yin [10] or Inoue et all [12].

The work of Han and Yin (analytically) allows *more* nonlinearity yet in presence of a *set of (approximating) restrictions* [cf. its page 188]. These authors characterize the context of their work to be “complicated” [page 189]. Still, from such a (“complicated”) context an analogue of the maximal (exhaustive; explicit and oblique) characterization presented in this paper does not emerge. A possible cause for such an issue appears to be the absence of some *structuring arguments* (needed to replace a “complicated” context by a *complex* context).

More nonlinearity is (numerically) allowed in the *parallel* interactions considered in the papers by Inoue et all or Grove and Menikoff.

2. LINEARIZED CONTEXT. INGREDIENTS OF A FOURIER–SNELL ANALYSIS

2.1. Linearized context

We begin by presenting the *linearized* context which will be used to describe the turbulence – shock interaction.

We consider, at the zeroth order of the linearization, a shock (= *admissible* discontinuity). A distinctive feature of the linearized analysis will be therefore that a *triad* is perturbed which includes, in addition to the adjacent (to the shock) constant (left/right) states u_l, u_r , the shock propagation speed D . If the perturbation is two-dimensional a linearized analysis has to begin with the system of equations

$$\frac{\partial u}{\partial t} + \frac{\partial f(u)}{\partial x} + \frac{\partial g(u)}{\partial y} = 0 \quad (2.1)$$

together with the jump conditions on the shock

$$[[u]] \frac{\partial \varphi}{\partial t} + [[f(u)]] \frac{\partial \varphi}{\partial x} + [[g(u)]] \frac{\partial \varphi}{\partial y} = 0 \quad (2.2)$$

where we put $[[u]] = u_r - u_l$ and, similarly, $[[f(u)]] = f(u_r) - f(u_l)$, etc.

We have to develop, with respect to a small parameter ε of the flow

$$0 < \varepsilon \ll \min(|u_r|, |u_l|) \quad \text{for } |u_r| \neq 0, |u_l| \neq 0,$$

both the dependent and independent variables in (2.1), (2.2). We express x, y, t in terms of X, Y, T (variables which are independent of ε) and ε , cf.

$$x = X + \varphi^\varepsilon(Y, T), \quad t = T, \quad y = Y; \quad \varphi^\varepsilon = DT + \psi^\varepsilon(Y, T) \quad (2.3)$$

use the independence of X, Y, T of ε in (2.3), assume that the perturbed data and the perturbed solution

$$u_0^\varepsilon(x, y) \equiv U_0^\varepsilon(X, Y; \varepsilon), \quad u^\varepsilon(x, y, t) \equiv U^\varepsilon(X, Y, T; \varepsilon)$$

smoothly depend on ε , and take into account

$$[U_{l,r}^\varepsilon]_{\varepsilon=0} = u_{l,r}, \quad [\psi^\varepsilon]_{\varepsilon=0} = 0, \quad \left[\frac{d}{d\varepsilon} U_0^\varepsilon \right]_{\varepsilon=0} = \tilde{U}_0, \quad \left[\frac{d}{d\varepsilon} U^\varepsilon \right]_{\varepsilon=0} = \tilde{U}, \quad \left[\frac{d}{d\varepsilon} \psi^\varepsilon \right]_{\varepsilon=0} = \psi;$$

then, separating the first order in ε , we are left with the linearized problem

$$\frac{\partial}{\partial T} \tilde{U} + A \frac{\partial}{\partial X} \tilde{U} + b \frac{\partial}{\partial Y} \tilde{U} = 0, \quad (X, Y) \in \mathbb{R}^2, \quad T > 0 \quad (2.4)$$

$$A_r \tilde{U}_r = A_l \tilde{U}_l + [[u]] \frac{\partial \psi}{\partial T} + [[g(u)]] \frac{\partial \psi}{\partial Y} \quad \text{for } X = 0 \quad (2.5)$$

$$\tilde{U}(X, Y, 0) = \tilde{U}_0(X, Y), \quad \psi(Y, 0) = \psi_0(Y), \quad (X, Y) \in \mathbb{R}^2 \quad (2.6)$$

where

$$A_{l,r} = a(u_{l,r}) - DI, \quad A = A(X) \equiv A_l[1 - H(X)] + A_r H(X); \quad a(u) = f'(u), \quad (2.7)$$

and b results from (2.7) when $A_{l,r}$ is replaced by $b(u_{l,r})$; H is the Heaviside function.

We notice that the limit $|u_r - u_l| \rightarrow 0$ of the linearized solution fulfils a linear problem; in fact, the limit linear problem *ignores* the contribution of ψ in the limit solution. This contribution could be regarded as a *memory* of an optimal context connected with the linearized problem. This aspect indicates the reality of a nonlinear subconscious. A nonlinear subconscious results when the nonlinearity is allowed only at the zeroth order of a perturbation expansion: we linearize the perturbation of a *piecewise constant* admissible solution and prove that the requirement of admissibility is still active at the first order and essentially structures the linearized description.

In the case of the *adiabatic gas dynamics of a perfect inviscid gas* the system (2.4) takes the form

$$\frac{1}{\bar{c}^2} \bar{\mathcal{D}} \tilde{p}_l + \bar{\rho} \frac{\partial \tilde{u}_l}{\partial X} + \bar{\rho} \frac{\partial \tilde{v}_l}{\partial Y} = 0, \quad \bar{\rho} \bar{\mathcal{D}} \tilde{u}_l + \frac{\partial \tilde{p}_l}{\partial X} = 0, \quad \bar{\rho} \bar{\mathcal{D}} \tilde{v}_l + \frac{\partial \tilde{p}_l}{\partial Y} = 0, \quad \bar{\mathcal{D}} \tilde{s}_l = 0 \quad \text{for } X < 0 \quad (2.8)$$

where

$$\tilde{p}_l = \bar{c}^2 \tilde{\rho}_l + (p_s)_l \tilde{s}_l \quad (2.9)$$

and

$$\mathcal{D} \tilde{p} + \frac{\partial \tilde{u}}{\partial X} + \frac{\partial \tilde{v}}{\partial Y} = 0, \quad \mathcal{D} \tilde{u} + \frac{\partial \tilde{p}}{\partial X} = 0, \quad \mathcal{D} \tilde{v} + \frac{\partial \tilde{p}}{\partial Y} = 0, \quad \mathcal{D} \tilde{s} = 0 \quad \text{for } X > 0 \quad (2.10)$$

where

$$\tilde{p} = \tilde{\rho} + (p_s)_r \tilde{s} \quad (2.11)$$

and we denote

$$\bar{\mathcal{D}} = \frac{\partial}{\partial T} + \bar{M} \frac{\partial}{\partial X} + M_y \frac{\partial}{\partial Y}, \quad \mathcal{D} = \frac{\partial}{\partial T} + M \frac{\partial}{\partial X} + M_y \frac{\partial}{\partial Y}.$$

Here, in usual notations, we put ρ, p, s, v_x, v_y for the density, pressure, specific entropy and velocity components respectively.

Relations (2.5) take in this case the form

$$(\tilde{s}_+, \tilde{p}_+, \tilde{u}_+, \tilde{v}_+)^t = \mathbf{a}(\tilde{s}_-, \tilde{p}_-, \tilde{u}_-, \tilde{v}_-)^t + \mathbf{b} \frac{\partial \psi}{\partial T} + \mathbf{c} \frac{\partial \psi}{\partial Y}, \quad \text{for } X = 0 \quad (2.12)$$

where $+/-$ indicate respectively the states behind/ahead of and, in presence of a component M_y in the direction Y for the velocity corresponding to the adjacent constant states, the coefficients $\mathbf{a}, \mathbf{b}, \mathbf{c}$ have the expressions

$$\left\{ \begin{array}{l} \mathbf{a}_{11} = 1 + \frac{\bar{M}}{2} \mathbf{b}_1, \quad \mathbf{a}_{12} = -\frac{(\gamma^2 - 1)^2}{2(\gamma + 1)} \cdot \frac{(M - \bar{M})^2}{2\gamma M^2 - (\gamma - 1)}, \quad \mathbf{a}_{13} = -\mathbf{b}_1, \\ \mathbf{a}_{21} = -\frac{2}{\gamma + 1} M \bar{M}, \quad \mathbf{a}_{22} = \frac{(\gamma + 1) - 2(\gamma - 1) M \bar{M}}{2\gamma M^2 - (\gamma - 1)}, \quad \mathbf{a}_{23} = -\mathbf{b}_2, \\ \mathbf{a}_{31} = M - \frac{\gamma - 1}{\gamma + 1} \bar{M}, \quad \mathbf{a}_{32} = \frac{2}{M} \cdot \frac{\gamma - 1}{\gamma + 1}, \quad \mathbf{a}_{33} = 1 - \mathbf{b}_3, \\ \mathbf{a}_{14} = \mathbf{a}_{24} = \mathbf{a}_{34} = \mathbf{a}_{41} = \mathbf{a}_{42} = \mathbf{a}_{43} = 0, \quad \mathbf{a}_{44} = 1, \\ \mathbf{b}_1 = -\frac{\gamma - 1}{M} \mathbf{c}_4^2, \quad \mathbf{b}_2 = -\frac{4M}{\gamma + 1}, \quad \mathbf{b}_3 = \frac{3 - \gamma}{\gamma + 1} + \frac{M}{\bar{M}}, \quad \mathbf{b}_4 = 0, \\ \mathbf{c}_1 = M_y \mathbf{b}_1, \quad \mathbf{c}_2 = M_y \mathbf{b}_2, \quad \mathbf{c}_3 = M_y \mathbf{b}_3, \quad \mathbf{c}_4 = \bar{M} - M. \end{array} \right.$$

We notice that the equations (2.8)–(2.12) are presented in a dimensionless form for which the entities of the perturbed flow are divided by the constant unperturbed state behind the shock. We denote by $\tilde{s}, \tilde{p}, \tilde{u}, \tilde{v}$ the dimensionless perturbation where

$$[x] = L, \quad [t] = \frac{L}{c_r}, \quad [\rho] = \rho_r, \quad [v] = c_r, \quad [p] = \rho_r c_r^2, \quad [s] = c_p, \quad [T] = \frac{c_r^2}{c_p}$$

$$M = \frac{v_{xr} - D}{[v]}, \quad \bar{M} = \frac{v_{xl} - D}{[v]}, \quad M_y = \frac{v_y}{[v]}, \quad \bar{\rho} = \frac{\rho_l}{[\rho]} = \frac{1}{\bar{\tau}}, \quad \bar{p} = \frac{p_l}{[p]}, \quad p = \frac{p_r}{[p]}, \quad \bar{c} = \frac{c_l}{[v]}.$$

2.2. Ingredients of a Fourier–Snell analysis

Two *essential, distinct* and *complementary* classes of *admissible (entropy)* solutions of (2.8)–(2.12) are considered in §§3–5: (a) solutions evolving from initial data which tend suitably fast to zero as $|X| \rightarrow \infty$, and, (b) elementary polymodal Fourier–Snell structures of a *real* frequency [an admissible elementary polymodal Fourier–Snell structure of a strictly complex frequency belongs to the class (a)]. It can be shown that the requirement of admissibility completely structures/determines the [linearized] solutions in each of these classes.

In the *multidimensional* case [in contrast with the one-dimensional case] the stability of these linearized solutions is not unconditionally guaranteed. A distinction between the stable and unstable circumstances is essentially made, in this case, by a *linearization criterion*: see Blokhin and Trakhinin [1] and Dinu [3] for a thorough review. Incidentally, in case of the adiabatic dynamics of a perfect inviscid gas the linearization appears to be active.

This paper aims to present an example of evolution in the class (a) still constructed as a superposition of elements in the class (b).

We complete the present paragraph with a short review of some aspects of a (linearized) Fourier–Snell analysis in presence of a shock (= admissible discontinuity).

In presence of an admissible discontinuity (shock) the role that a modal monochromatic wave plays in a linear Fourier analysis is taken over, in a *linearized* Fourier type analysis, by an elementary polymodal structure. Such an elementary structure consists in a *finite* (eventually *minimal*) number of *Snell compatible* monochromatic waves.

A monochromatic wave has the form

$$(\tilde{s}_{l,r}, \tilde{p}_{l,r}, \tilde{u}_{l,r}, \tilde{v}_{l,r})^t = (\hat{s}_{l,r}, \hat{p}_{l,r}, \hat{u}_{l,r}, \hat{v}_{l,r})^t \exp i(\alpha_{l,r} X + \beta_{l,r} Y - \omega_{l,r} T), \quad \beta_{l,r} \in \mathbb{R},$$

associated with the propagation vector

$$(\alpha_{l,r}, \beta_{l,r}) = k_{l,r} (\cos \kappa_{l,r}, \sin \kappa_{l,r}).$$

As is well known, there are three gasdynamic distinct modes: a sound mode and a (double) entropy–vorticity mode; therefore, we have at our disposal six modal monochromatic waves (three for each of the two regions adjacent to the shock) to construct an elementary structure and we use, as a *key* element of this construction the following Snell laws of refraction through/reflection at the shock:

- all the monochromatic waves implied in the elementary structure have
- (S₁) equal frequencies ω , when measured in the same reference frame, and
- (S₂) equal values of β .

Essentially, for the monochromatic waves which contribute in an elementary structure, we use in this construction: the shock relations (2.12) to connect their amplitudes and the mentioned

Snell laws (S_1), (S_2) to connect, via the modal dispersion laws, their propagation vectors.

The class (b) of elementary structures is presented in our study as an union of two disjoint subclasses (see for example Kontorovich [13], Dinu [3]) : a *pseudohyperbolic* subclass [each element of this subclass includes only monochromatic waves with a real α], and, a *pseudoelliptic* subclass [each element of this subclass has a structure which includes at least a monochromatic wave with a (strictly) complex α]. It can be proven that only four [real frequency] elementary structures are admissible [= have a completely determined/organized linearized evolution] in presence of an admissible discontinuity (see for example Kontorovich [13], Dinu [3]); precisely:

$$\mathcal{V}_{li}^+ \mathcal{S}_{rd}^+ \mathcal{V}_{rd}, \quad \mathcal{S}_{li}^+ \mathcal{S}_{rd}^+ \mathcal{V}_{rd}, \quad \mathcal{S}_{li}^- \mathcal{S}_{rd}^- \mathcal{V}_{rd}, \quad \mathcal{S}_{ri}^- \mathcal{S}_{rd}^+ \mathcal{V}_{rd}, \quad (2.13)$$

where in (2.13) \mathcal{V} and \mathcal{S} indicate, respectively, an entropy–vorticity [ahead of the shock: entropy and/or vorticity] and a sound contribution [with the subscripts l/r for left (ahead of; in our study we consider a backward shock wave)/right (behind), and i/d for incident/divergent (emergent)]. In other words, each elementary polymodal structure fulfills the part (2.8)–(2.12) of the linearized problem and the interaction solution of (2.6), (2.8)–(2.12) is Fourier–Snell represented/constructed as a superposition of certain [admissible, real frequency] elementary polymodal structures. We have to notice in this respect that in a refraction passage the emergent initial data in (2.6) result constructively from the Fourier representation of the incident initial data.

The present paper only considers the details related to the first of the elements (elementary structures) (2.13). If we associate, as a parameter, to this element the inclination of its incident entropy–vorticity propagation vector, cf.

$$\mathfrak{z} = \tan \kappa_{ev,li} = \frac{\beta}{\alpha_{ev,li}} = -\cot \phi_l, \quad (2.14)$$

(see Figure 1) then it can be shown that two cases, a pseudohyperbolic one [for $|\mathfrak{z}| < \mathfrak{z}_c$] and respectively a pseudoelliptic one [for $|\mathfrak{z}| > \mathfrak{z}_c$], are possible for the considered structure, separated by the critical value

$$\mathfrak{z}_c = \frac{\overline{M}}{\sqrt{1 - M^2}}. \quad (2.14)_c$$

The structures (2.13) replace the four elementary (monochromatic) waves of the gasdynamic Fourier theory of a *linear* problem.

3. THE RIBNER PARALLEL LINEARIZED SOLUTION

3.1. Highlights of this work

Paragraphs 3–5 present (thus materializing a suggestion of §1) a *set of arguments needed to structure* the complex construction of the interaction (turbulence–shock) solution. Paragraphs 3,4 consider a *parallel* version (see §1) of the mentioned set of arguments. Then, an *oblique* version of this set of arguments is taken into account in §5.

3.2. Sound contribution in the interaction solution: first constructive details. Gasdynamic partitions (I)

We shall use the Lagrangian reference frames $\underline{x}, \underline{y}$ (fixed on the undisturbed flow ahead of the shock) and \tilde{x}, \tilde{y} (fixed on the undisturbed flow behind the shock) in addition to the frame X, Y

fixed on the shock discontinuity. We have

$$\underline{x} = X - \overline{M}T, \quad \underline{\tilde{x}} = X - MT = \underline{x} + (\overline{M} - M)\underline{\tilde{t}}; \quad \underline{y} = \underline{\tilde{y}} = Y; \quad \underline{t} = \underline{\tilde{t}} = T. \quad (3.1)$$

Now, in the frame $\underline{x}, \underline{y}$ we consider for the subsystem (2.8), (2.9) the *steady* solution of a vortex with a *finite* core

$$[\underline{\tilde{u}}(\underline{x}, \underline{y}), \underline{\tilde{v}}(\underline{x}, \underline{y})] = \frac{\underline{\tilde{\varepsilon}}}{2\pi} \begin{cases} (1/r_*^2)[- \underline{y}, \underline{x}] & \text{for } r \leq r_* \\ (1/r^2)[- \underline{y}, \underline{x}] & \text{for } r_* \leq r \end{cases}, \quad \underline{\tilde{s}} \equiv \underline{\tilde{p}} \equiv 0 \quad (3.2)$$

where r_* is the radius of the vortex core.

PROPOSITION 3.1 (Ribner [15]). *The solution (3.2) is Fourier represented by*

$$\{\underline{\tilde{s}}, \underline{\tilde{p}}, \underline{\tilde{u}}, \underline{\tilde{v}}\} = -\frac{\underline{\tilde{\varepsilon}}}{2\pi^2} \text{Im} \int_0^\infty \frac{1}{k} \cdot \frac{2J_1(kr_*)}{kr_*} dk \int_{-\pi/2}^{\pi/2} \exp[i(\alpha_l \underline{x} + \beta_l \underline{y})] \{0, 0, \beta_l, -\alpha_l\} d\kappa_l. \quad (3.3)$$

□

Remark 3.2 (Ribner [15]). (i) The parallel vortex–shock interaction solution results cf. (3.3) and (2.13)₁. Precisely: we have to complete, in the region behind the shock, each incident vorticity wave in the sum (3.3) up to an elementary structure (2.13)₁. Therefore, a sound contribution and, respectively, an entropy–vorticity contribution are seen to be included by the mentioned interaction solution in the region behind the shock. Only the emergent sound contribution will be *constructed*. The emergent entropy–vorticity contribution will be then *represented* in terms of the emergent sound contribution [see (3.8)–(3.11) here in below]. (ii) We notice (Figure 1) that to *each* elementary structure (2.13)₁ which contributes in the representation of the interaction solution an associated frame \widehat{X}, \widehat{Y} corresponds which translates along the shock, cf. $\widehat{X} = X, \widehat{Y} = Y + M_y T$, where the velocity M_y is chosen [to annul the frequency of the incident vorticity wave] so as to make steady the elementary structure (2.13)₁ associated to it. □

We compute:

$$\alpha_l \underline{x} + \beta_l \underline{y} = \alpha_l \widehat{X} + \beta_l \widehat{Y}.$$

Now, the emergent *sound* monochromatic wave corresponding to the incident vorticity monochromatic wave

$$A_0(0, 0, \beta_l, -\alpha_l) \exp[i(\alpha_l \underline{x} + \beta_l \underline{y})] \\ A_0 = -\frac{\underline{\tilde{\varepsilon}}}{2\pi^2} \cdot \frac{2J_1(kr_*)}{kr_*} \cdot \frac{1}{k} dk d\kappa_l = -\frac{\underline{\tilde{\varepsilon}}}{2\pi^2} \cdot \frac{2J_1(kr_*)}{kr_*} \cdot \frac{1}{k} \cdot \frac{1}{1 + \mathfrak{z}^2} dk d\mathfrak{z}$$

in (3.3) can be presented by:

$$A_1[0, -(M\alpha_s + M_y\beta_l), \alpha_s, \beta_l] \exp[i(\alpha_s \widehat{X} + \beta_l \widehat{Y})], \quad A_1 = a_1 A_0 \\ a_1 = \mathfrak{z} \frac{(d_{11}\mathfrak{z}^2 + d_{12}) + (d_{13}\mathfrak{z}^2 + d_{14})\check{\varepsilon}\sqrt{|\mathfrak{z}_c^2 - \mathfrak{z}^2|}}{(d_{01}\mathfrak{z}^2 + d_{02}) + (d_{03}\mathfrak{z}^2 + d_{04})\check{\varepsilon}\sqrt{|\mathfrak{z}_c^2 - \mathfrak{z}^2|}}, \quad \check{\varepsilon} = \begin{cases} 1 & \text{for } |\mathfrak{z}| \leq \mathfrak{z}_c \\ i & \text{for } |\mathfrak{z}| \geq \mathfrak{z}_c \end{cases} \quad (3.4)$$

with

$$\begin{aligned} d_{01} &= \frac{2}{\gamma+1} \frac{\overline{M}}{M} (1-2M^2), \quad d_{02} = \frac{\overline{M}}{M} d_{01} - \frac{8}{(\gamma+1)^2} \frac{\overline{M}^2}{M^2} (1-M^2) \\ d_{03} &= -\frac{2}{\gamma+1} \sqrt{1-M^2}, \quad d_{04} = \frac{\overline{M}}{M} d_{03}, \\ d_{11} &= \frac{8}{(\gamma+1)^2} (1-M^2), \quad d_{12} = -\frac{\overline{M}}{M} d_{11}, \quad d_{13} = d_{14} = 0 \end{aligned}$$

where we use the *Lorentz coordinates*

$$x = \frac{\tilde{x} + M\tilde{t}}{\sqrt{1-M^2}} = \frac{X}{\sqrt{1-M^2}}, \quad y = \tilde{y}, \quad t = \frac{\tilde{t} + M\tilde{x}}{\sqrt{1-M^2}} \quad (3.5)$$

to compute, cf. (2.14), (3.1) and Remark 3.2(ii):

$$\begin{aligned} \frac{\alpha_s}{\beta_l} = \mu &= \begin{cases} \frac{\sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - M\mathfrak{z}_c}{\mathfrak{z}\sqrt{1-M^2}} & \text{for } |\mathfrak{z}| < \mathfrak{z}_c \\ \frac{i\sqrt{\mathfrak{z}^2 - \mathfrak{z}_c^2} - M\mathfrak{z}_c}{\mathfrak{z}\sqrt{1-M^2}} & \text{for } \mathfrak{z}_c < |\mathfrak{z}| \end{cases} \\ i(\alpha_s \widehat{X} + \beta_l \widehat{Y}) &= \begin{cases} k \frac{x\sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - (t\mathfrak{z}_c - y\mathfrak{z})}{\sqrt{1+\mathfrak{z}^2}} & \text{for } |\mathfrak{z}| \leq \mathfrak{z}_c \\ -k \frac{x\sqrt{\mathfrak{z}^2 - \mathfrak{z}_c^2}}{\sqrt{1+\mathfrak{z}^2}} - ik \frac{t\mathfrak{z}_c - y\mathfrak{z}}{\sqrt{1+\mathfrak{z}^2}} & \text{for } |\mathfrak{z}| \geq \mathfrak{z}_c. \end{cases} \end{aligned}$$

The **sound** contribution in the constructed solution for $X > 0$ (behind the shock) results from (3.3), (2.14) and (3.5) cf. Remark 3.2(i) and consists of a **pseudohyperbolic** part, abbreviated *h*-part, which is a superposition (Figure 1a,b) of pseudohyperbolic waves corresponding to $|\mathfrak{z}| \leq \mathfrak{z}_c$,

$$\begin{aligned} &[\tilde{p}_h(x, y, t), \tilde{u}_h(x, y, t), \tilde{v}_h(x, y, t)] \\ &= \frac{\tilde{\varepsilon}}{2\pi^2} \int_{-\mathfrak{z}_c}^{\mathfrak{z}_c} \mathcal{I}_h(r_*) \left[\frac{M\sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - \mathfrak{z}_c}{\mathfrak{z}\sqrt{1-M^2}}, -\frac{\sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - M\mathfrak{z}_c}{\mathfrak{z}\sqrt{1-M^2}}, -1 \right] \cdot a_1 \cdot \frac{\mathfrak{z}}{\sqrt{1+\mathfrak{z}^2}} \cdot \frac{1}{1+\mathfrak{z}^2} d\mathfrak{z} \quad (3.6) \end{aligned}$$

$$\mathcal{I}_h(r_*) = \int_0^\infty \frac{2J_1(kr_*)}{kr_*} \sin \left[k \frac{x\sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - (t\mathfrak{z}_c - y\mathfrak{z})}{\sqrt{1+\mathfrak{z}^2}} \right] dk \quad (3.6)^*$$

and a **pseudoelliptic** part, abbreviated *e*-part, which is a superposition of pseudoelliptic waves corresponding to $|\mathfrak{z}| \geq \mathfrak{z}_c$,

$$\begin{aligned} &[\tilde{p}_e(x, y, t), \tilde{u}_e(x, y, t), \tilde{v}_e(x, y, t)] \\ &= \frac{\tilde{\varepsilon}}{2\pi^2} \text{Im} \left(\int_{-\infty}^{-\mathfrak{z}_c} + \int_{\mathfrak{z}_c}^{\infty} \right) \mathcal{I}_e(r_*) \left[\frac{iM\sqrt{\mathfrak{z}^2 - \mathfrak{z}_c^2} - \mathfrak{z}_c}{\mathfrak{z}\sqrt{1-M^2}}, -\frac{i\sqrt{\mathfrak{z}^2 - \mathfrak{z}_c^2} - M\mathfrak{z}_c}{\mathfrak{z}\sqrt{1-M^2}}, -1 \right] \cdot a_1 \cdot \frac{\mathfrak{z}}{\sqrt{1+\mathfrak{z}^2}} \cdot \frac{1}{1+\mathfrak{z}^2} d\mathfrak{z} \quad (3.7) \end{aligned}$$

$$\mathcal{I}_e(r_*) = \int_0^\infty \frac{2J_1(kr_*)}{kr_*} \exp \left[-k \frac{x\sqrt{\mathfrak{z}^2 - \mathfrak{z}_c^2}}{\sqrt{1+\mathfrak{z}^2}} - ik \frac{t\mathfrak{z}_c - y\mathfrak{z}}{\sqrt{1+\mathfrak{z}^2}} \right] dk. \quad (3.7)^*$$

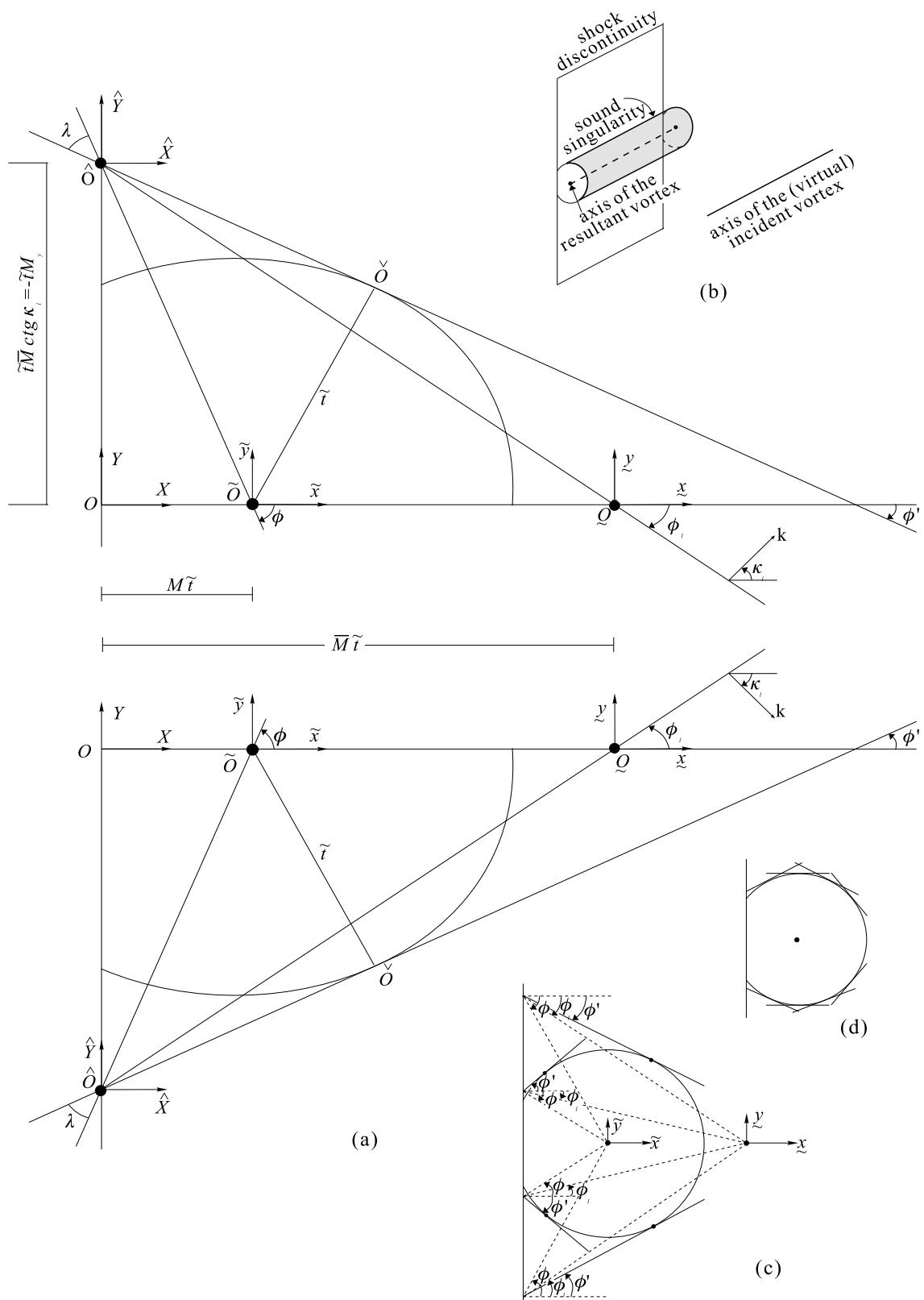


FIGURE 1 Details of the parallel construction

The form (3.6), (3.7) reflects some essential rearrangements (see Dinu [2], [3]) of the original Ribner's representation.

We could obtain expressions similar to (3.6), (3.7) for the *entropy–vorticity* contribution and the *shock disturbance*. Still, we shall prefer, using the equations (2.8)–(2.11) and the shock relations (2.12), to represent these contributions in terms of the sound contribution cf.:

$$\begin{aligned} & \tilde{u}_{\text{vorticity}}(\tilde{x}, \tilde{y}, \tilde{t}) \\ &= \tilde{u}_-\left(\tilde{y}, \tilde{t} = T - \frac{X}{M}\right) + \frac{b_3}{b_2} \tilde{p}_+\left(\tilde{y}, \tilde{t} = T - \frac{X}{M}\right) - \int_{T - \frac{X}{M}}^T \frac{\partial \tilde{p}}{\partial \tilde{x}}(\tilde{x}, \tilde{y}, \theta) d\theta - \tilde{u}_{\text{sound}}(\tilde{x}, \tilde{y}, \tilde{t}) \quad (3.8) \end{aligned}$$

$$\begin{aligned} & \tilde{v}_{\text{vorticity}}(\tilde{x}, \tilde{y}, \tilde{t}) \\ &= \tilde{v}_-\left(\tilde{y}, \tilde{t} = T - \frac{X}{M}\right) + c_4 \frac{\partial \psi}{\partial \tilde{y}}\left(\tilde{y}, \tilde{t} = T - \frac{X}{M}\right) - \int_{T - \frac{X}{M}}^T \frac{\partial \tilde{p}}{\partial \tilde{y}}(\tilde{x}, \tilde{y}, \theta) d\theta - \tilde{v}_{\text{sound}}(\tilde{x}, \tilde{y}, \tilde{t}) \quad (3.9) \end{aligned}$$

$$\tilde{s}(\tilde{x}, \tilde{y}, \tilde{t}) \equiv \frac{b_1}{b_2} \tilde{p}_+\left(-\frac{\tilde{x}}{M}, \tilde{y}\right) \quad (3.10)$$

$$\psi(\tilde{y}, \tilde{t}) = \int_{-\infty}^{\tilde{t}} \left[\frac{1}{b_2} \tilde{p}_+(\tilde{y}, \theta) + \tilde{u}_-(\tilde{y}, \theta) \right] d\theta \quad (3.11)$$

where we have to insert in (3.8), (3.9), cf. (3.1)

$$T = \tilde{t}, \quad T - \frac{X}{M} = -\frac{\tilde{x}}{M}, \quad \tilde{y} = \tilde{y},$$

and we take into account that $\lim_{T \rightarrow -\infty} \psi = 0$ in order to get (3.11).

We motivate by Remark 3.2 to call (3.2), (3.6), (3.7), (3.8)–(3.11) *the Ribner representation of the linearized interaction solution*.

4. EXPLICIT FORM OF RIBNER'S REPRESENTATION

4.1. Two essential elements of the structural analysis

Before presenting the details of the analysis in this paragraph we have to identify, cf. Terminology 4.1 here below, two elements essential for structuring this analysis. We denote in (3.6)*

$$\begin{aligned} \mathcal{E}(\tilde{x}, \tilde{y}, \tilde{t}; \mathfrak{z}) &\stackrel{\text{def}}{=} x \sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - (t \mathfrak{z}_c - y \mathfrak{z}) \\ &\equiv \frac{\tilde{x}(\sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - M \mathfrak{z}_c) + \tilde{y} \mathfrak{z} \sqrt{1 - M^2} + \tilde{t}(M \sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2} - \mathfrak{z}_c)}{\sqrt{1 - M^2}}, \quad \mathfrak{z} \in (-\mathfrak{z}_c, \mathfrak{z}_c). \end{aligned}$$

A straightforward calculation shows that for each $\tilde{t} > 0$ the envelope (corresponding to the *pseudohyperbolic* contribution; depicted, cf. Figure 1, in X, Y with T as a parameter) of the straightlines family $\mathcal{E} = 0$, $\mathfrak{z} \in (-\mathfrak{z}_c, \mathfrak{z}_c)$ has the form of an *arc* of the (dimensionless) *sonic circle*

$$\tilde{x}^2 + \tilde{y}^2 - \tilde{t}^2 = x^2 + y^2 - t^2 = 0, \quad X > 0. \quad (4.1)$$

TERMINOLOGY 4.1 (Ribner [15]). *We shall call the arc (4.1) the S -arc; also, we shall call the region of the sonic disk belonging to the half-plane $X > 0$ the S -region.*

4.2. The highlights of the parallel analysis

Remark 4.2. We have $\mathcal{E}(\tilde{x}, \tilde{y}, \tilde{t}; \mathfrak{z}) < 0$, $\mathfrak{z} \in (-\mathfrak{z}_c, \mathfrak{z}_c)$ at the interior points of the S -region. Consequently, the phase in (3.6)* is (strictly) negative at the interior points of the S -region. \square

At this point we have to notice that even in presence of the structuring arguments of §3 we may need a bit of “chance” in order to get a successful calculation in the Ribner representation. For example, the attempt to obtain an explicit/closed form for the Ribner *parallel* interaction solution may be fruitless if we are not aware of the presence of a lot of “traps”: (i) the emergent sound contribution (3.6), (3.7) cannot be computed *directly*; in fact, this contribution can be put in an explicit form directly *only* in the limit $r_* \rightarrow 0$ and *only* at the points of the S -region; incidentally it can be predicted (and verified) at the exterior points of the S -region; (ii) the emergent entropy–vorticity contribution cannot be computed directly in its Fourier–Snell representation [similar to (3.6), (3.7)] even in the limit $r_* \rightarrow 0$; its explicit form results by taking into account its connection (3.8)–(3.11) with the emergent sound contribution; (iii) finally, the explicit form of the Ribner nonsingular interaction representation results from a *re-weighting* (a re-set of the weight lost in the limit $r_* \rightarrow 0$; cf. Dinu and Dinu [6]).

4.3. Gasdynamic factorizations (I)

Remark 4.3 (Dinu [2]). By rationalizing the denominator of (3.4) we obtain, irrespectively of the circumstances $|\mathfrak{z}| \leq \mathfrak{z}_c$ or $|\mathfrak{z}| \geq \mathfrak{z}_c$, the *factorized* expression

$$E(\mathfrak{z}^2) \stackrel{\text{def}}{=} (d_{01}\mathfrak{z}^2 + d_{02})^2 + (d_{03}\mathfrak{z}^2 + d_{04})^2(\mathfrak{z}^2 - \mathfrak{z}_c^2) \equiv d_{03}^2(\mathfrak{z}^2 + a^2)(\mathfrak{z}^2 - b^2)(\mathfrak{z}^2 - c^2) \quad (4.2)$$

where

$$a \stackrel{\text{def}}{=} \frac{\overline{M}}{M}, \quad \varpi_{\pm}^2 \stackrel{\text{def}}{=} \frac{\overline{M}}{M} \left[(2M\overline{M} - 1) \pm 2M\sqrt{\frac{\gamma - 1}{\gamma + 1}M\overline{M}} \right], \quad b^2 \stackrel{\text{def}}{=} \varpi_-^2, \quad c^2 \stackrel{\text{def}}{=} \varpi_+^2 \quad (4.3)$$

$$a > 1, \quad \begin{cases} b^2 > 0 & \text{for } -1 < \gamma < \frac{5}{3}; \\ 0 < |b| < |c| < \mathfrak{z}_c & \end{cases} \quad c^2 > 0 \quad (4.4)$$

where a corresponds to the entropy–vorticity contribution while b, c correspond to the sound contribution. \square

4.4 Singular limit of the sound contribution: the first details

The computation of the limit $r_* \rightarrow 0$ of the sound contribution begins with the following steps.

■ (†) We explicitly calculate $\mathcal{I}_h(r_*)$, $\mathcal{I}_e(r_*)$, given by (3.6)*, (3.7)*, and then $\lim_{r_* \rightarrow 0} \mathcal{I}_h(r_*)$, $\lim_{r_* \rightarrow 0} \mathcal{I}_e(r_*)$ at the points of the S -region (using the Remark 4.2). We have from (3.6)* for each interior point of the S -region:

$$\mathcal{I}_h(r_*) = -\frac{2\sqrt{1+\mathfrak{z}^2}}{|x\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}-(t\mathfrak{z}_c-y\mathfrak{z})| + \sqrt{|x\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}-(t\mathfrak{z}_c-y\mathfrak{z})|^2-r_*^2(1+\mathfrak{z}^2)}}$$

and then

$$\lim_{r_* \rightarrow 0} \mathcal{I}_h(r_*) = \frac{\sqrt{1+\mathfrak{z}^2}}{x\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}-(t\mathfrak{z}_c-y\mathfrak{z})} = -\frac{\sqrt{1+\mathfrak{z}^2}}{x^2+y^2} \cdot \frac{x\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}+(t\mathfrak{z}_c-y\mathfrak{z})}{(\mathfrak{z}-\xi)^2+\eta^2}.$$

A similar calculation gives for each interior point of the S -region:

$$\lim_{r_* \rightarrow 0} \mathcal{I}_e(r_*) = \frac{\sqrt{1+\mathfrak{z}^2}}{x^2+y^2} \cdot \frac{x\sqrt{\mathfrak{z}^2-\mathfrak{z}_c^2}-i(t\mathfrak{z}_c-y\mathfrak{z})}{(\mathfrak{z}-\xi)^2+\eta^2}.$$

■ (‡) We use the calculations (†) and the factorization (4.2) to get the limit $r_* \rightarrow 0$ of the sound component (3.6), (3.7) at the points of the S -region. We denote

$$\xi = \frac{\mathfrak{z}_c t y}{x^2+y^2}, \quad \eta = \frac{\mathfrak{z}_c x \sqrt{t^2-x^2-y^2}}{x^2+y^2}$$

$$K = \frac{1}{\pi\sqrt{1-M^2}} \bar{K}, \quad \bar{K} = \frac{\tilde{\varepsilon}}{2\pi} \cdot \frac{1}{d_{03}^2}$$

$$Q_1(\mathfrak{z}^2) \stackrel{\text{def}}{=} d_{11}\mathfrak{z}^2 + d_{12}, \quad Q_2(\mathfrak{z}^2) \stackrel{\text{def}}{=} d_{01}\mathfrak{z}^2 + d_{02}, \quad Q_3(\mathfrak{z}^2) \stackrel{\text{def}}{=} d_{03}\mathfrak{z}^2 + d_{04}$$

to obtain at the points of the S -region:

$$\begin{aligned} & [\tilde{p}_h(x, y, t), \tilde{u}_h(x, y, t), \tilde{v}_h(x, y, t)] \\ &= -\frac{K}{x^2+y^2} \int_{-\mathfrak{z}_c}^{\mathfrak{z}_c} \frac{x\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}+(t\mathfrak{z}_c-y\mathfrak{z})}{(\mathfrak{z}-\xi)^2+\eta^2} \\ & \quad \cdot \left[(M\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}-\mathfrak{z}_c), -(\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}-M\mathfrak{z}_c), -\mathfrak{z}\sqrt{1-M^2} \right] \\ & \quad \cdot \frac{\mathfrak{z}Q_1(\mathfrak{z}^2)[Q_2(\mathfrak{z}^2)-Q_3(\mathfrak{z}^2)\sqrt{\mathfrak{z}_c^2-\mathfrak{z}^2}]}{(\mathfrak{z}^2+a^2)(\mathfrak{z}^2-b^2)(\mathfrak{z}^2-c^2)(\mathfrak{z}^2+1)} d\mathfrak{z} \end{aligned} \quad (4.5)$$

$$\begin{aligned} & [\tilde{p}_e(x, y, t), \tilde{u}_e(x, y, t), \tilde{v}_e(x, y, t)] \\ &= \frac{K}{x^2+y^2} \text{Im} \left(\int_{-\infty}^{-\mathfrak{z}_c} + \int_{\mathfrak{z}_c}^{\infty} \right) \frac{x\sqrt{\mathfrak{z}^2-\mathfrak{z}_c^2}-i(t\mathfrak{z}_c-y\mathfrak{z})}{(\mathfrak{z}-\xi)^2+\eta^2} \\ & \quad \cdot \left[(iM\sqrt{\mathfrak{z}^2-\mathfrak{z}_c^2}-\mathfrak{z}_c), -(i\sqrt{\mathfrak{z}^2-\mathfrak{z}_c^2}-M\mathfrak{z}_c), -\mathfrak{z}\sqrt{1-M^2} \right] \\ & \quad \cdot \frac{\mathfrak{z}Q_1(\mathfrak{z}^2)[Q_2(\mathfrak{z}^2)-iQ_3(\mathfrak{z}^2)\sqrt{\mathfrak{z}^2-\mathfrak{z}_c^2}]}{(\mathfrak{z}^2+a^2)(\mathfrak{z}^2-b^2)(\mathfrak{z}^2-c^2)(\mathfrak{z}^2+1)} d\mathfrak{z}. \end{aligned} \quad (4.6)$$

4.5. Gasdynamic factorizations (II). Gasdynamic partitions (II)

We notice that the representations (4.5), (4.6) have a most suggestive form. They present, for example, through distinct factors, the contribution of the *vortex shape* and the contribution of the *shock-vorticity interaction*; these contributions are connected to the factors $[(\mathfrak{z} - \xi)^2 + \eta^2]$ or, respectively, $(\mathfrak{z}^2 - \zeta_i)$, $1 \leq i \leq 4$ where we denote, cf. (4.3), (4.4),

$$\zeta_1 = -a^2, \quad \zeta_2 = b^2, \quad \zeta_3 = c^2, \quad \zeta_4 = -1.$$

We shall add to the partition (3.6), (3.7) a new partition to distinguish between the contribution of the *vortex shape* (label *vs*) and that of the *shock-vorticity interaction* (label *int*); such a partition will take into account the decompositions

$$\begin{aligned} & \frac{1}{[(\mathfrak{z} - \xi)^2 + \eta^2](\mathfrak{z}^2 - \zeta_i)} \\ &= \frac{1}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2\zeta_i} \left\{ \frac{(-2\xi)\mathfrak{z} + (3\xi^2 - \eta^2 - \zeta_i)}{(\mathfrak{z} - \xi)^2 + \eta^2} + \frac{(2\xi)\mathfrak{z} + (\xi^2 + \eta^2 + \zeta_i)}{\mathfrak{z}^2 - \zeta_i} \right\} \\ & \frac{\mathfrak{z}}{[(\mathfrak{z} - \xi)^2 + \eta^2](\mathfrak{z}^2 - \zeta_i)} \\ &= \frac{1}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2\zeta_i} \left\{ \frac{-(\xi^2 + \eta^2 + \zeta_i)\mathfrak{z} + 2\xi(\xi^2 + \eta^2)}{(\mathfrak{z} - \xi)^2 + \eta^2} + \frac{(\xi^2 + \eta^2 + \zeta_i)\mathfrak{z} + (2\xi\zeta_i)}{\mathfrak{z}^2 - \zeta_i} \right\}. \end{aligned}$$

The expression $[(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2\zeta_i]$ is then revealed as a price paid for separation or, as a *memory* of this separation. It allows a *second gasdynamic factorization* [which uses (3.5)]

$$(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2\zeta_i = \frac{1}{(x^2 + y^2)^2} [(\mathfrak{z}_c t - x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2][(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2]. \quad (4.7)$$

We briefly present the succession of the two mentioned partitions by

$$[\tilde{p}, \tilde{u}, \tilde{v}] = [\tilde{p}_h, \tilde{u}_h, \tilde{v}_h] + [\tilde{p}_e, \tilde{u}_e, \tilde{v}_e] = [\tilde{p}_{vs}, \tilde{u}_{vs}, \tilde{v}_{vs}] + [\tilde{p}_{int}, \tilde{u}_{int}, \tilde{v}_{int}]. \quad (4.8)$$

4.6. Some calculation details

The list of integrals corresponding to the *vs*-part consists of

$$[\mathcal{I}_0(\xi, \eta^2), \mathcal{I}_1(\xi, \eta^2)] = \int_{-\infty}^{\infty} \frac{[1, \mathfrak{z}]}{(\mathfrak{z} - \xi)^2 + \eta^2} d\mathfrak{z} = \frac{\pi}{\eta} [1, \xi] \quad (4.9)$$

$$\begin{aligned} [\mathcal{K}_0(\xi, \eta^2), \mathcal{K}_1(\xi, \eta^2)] &= \int_{-\mathfrak{z}_c}^{\mathfrak{z}_c} \frac{[1, \mathfrak{z}]}{\sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2}[(\mathfrak{z} - \xi)^2 + \eta^2]} d\mathfrak{z} \\ &= \frac{1}{\eta\sqrt{2}} \cdot \frac{\sqrt{(\mathfrak{z}_c^2 + \eta^2 - \xi^2) + \sqrt{(\mathfrak{z}_c^2 + \eta^2 - \xi^2)^2 + 4\xi^2\eta^2}}}{\sqrt{(\mathfrak{z}_c^2 + \eta^2 - \xi^2)^2 + 4\xi^2\eta^2}} \\ &\quad \cdot \left[\frac{2\xi}{(\mathfrak{z}_c^2 + \eta^2 - \xi^2) + \sqrt{(\mathfrak{z}_c^2 + \eta^2 - \xi^2)^2 + 4\xi^2\eta^2}}, 1 \right] \\ &= \frac{1}{\mathfrak{z}_c^3} \cdot \frac{x^2 + y^2}{(t^2 - y^2)\sqrt{t^2 - x^2 - y^2}} [y, \mathfrak{z}_c t] \end{aligned} \quad (4.10)$$

$$[\mathcal{J}_0(\xi, \eta^2), \mathcal{J}_1(\xi, \eta^2), \mathcal{J}_2(\xi, \eta^2)] = \int_{-\mathfrak{z}_c}^{\mathfrak{z}_c} \frac{[1, \mathfrak{z}, \mathfrak{z}^2] \sqrt{\mathfrak{z}_c^2 - \mathfrak{z}^2}}{(\mathfrak{z} - \xi)^2 + \eta^2} d\mathfrak{z} = [\mathcal{J}_0^r, \mathcal{J}_1^r, \mathcal{J}_2^r] + [\mathcal{J}_0^s, \mathcal{J}_1^s, \mathcal{J}_2^s] \quad (4.11)$$

$$\left\{ \begin{array}{l} [\mathcal{J}_0^r, \mathcal{J}_1^r, \mathcal{J}_2^r] = \pi \left[-1, -2\xi, \frac{1}{2}\mathfrak{z}_c^2 - 3\xi^2 + \eta^2 \right] \\ [\mathcal{J}_0^s, \mathcal{J}_1^s, \mathcal{J}_2^s] = -\pi\mathfrak{z}_c^2 [2\xi, 3\xi^2 - \eta^2 - \mathfrak{z}_c^2, 2\xi(2\xi^2 - 2\eta^2 - \mathfrak{z}_c^2)] \mathcal{K}_0 \\ \quad + \pi[\xi^2 + \eta^2 + \mathfrak{z}_c^2, 2\xi(\xi^2 + \eta^2), (\xi^2 + \eta^2)(3\xi^2 - \eta^2 - \mathfrak{z}_c^2)] \mathcal{K}_1 \end{array} \right. \quad (4.11)_{r,s}$$

$$\left\{ \begin{array}{l} \mathcal{J}_0^s = \frac{t}{\sqrt{t^2 - x^2 - y^2}}, \quad \mathcal{J}_1^s = \frac{y}{\sqrt{t^2 - x^2 - y^2}} \cdot \frac{\mathfrak{z}_c}{x^2 + y^2} (2t^2 - x^2 - y^2), \\ \mathcal{J}_2^s = \frac{t}{\sqrt{t^2 - x^2 - y^2}} \left(\frac{\mathfrak{z}_c}{x^2 + y^2} \right)^2 [t^2(3y^2 - x^2) - (x^2 + y^2)(2y^2 - x^2)]. \end{array} \right. \quad (4.11)_s$$

We complete this list by using the remark that if η^2 is replaced by $(-\bar{\eta}^2)$ in (4.9)–(4.11) then we get

$$\left\{ \begin{array}{l} \mathcal{I}_0(\xi, -\bar{\eta}^2) = 0, \quad \mathcal{I}_1(\xi, -\bar{\eta}^2) = 0, \\ \mathcal{K}_0(\xi, -\bar{\eta}^2) = 0, \quad \mathcal{K}_1(\xi, -\bar{\eta}^2) = 0, \end{array} \right. \quad (4.12)$$

$$\mathcal{J}_0^s(\xi, -\bar{\eta}^2) = 0, \quad \mathcal{J}_1^s(\xi, -\bar{\eta}^2) = 0, \quad \mathcal{J}_2^s(\xi, -\bar{\eta}^2) = 0. \quad (4.13)$$

A list similar to (4.9)–(4.11) can be shown for the *int*-part; the integrals of this list result from (4.9)–(4.13) when the details concerning the form of ζ_i , $1 \leq i \leq 4$, are taken into consideration cf. (4.3), (4.4). We have, for $1 \leq i \leq 4$,

$$\bar{\mathcal{I}}_0(\zeta_i) = \mathcal{I}_0(0, -\zeta_i) = (2-i)(3-i) \frac{\pi}{2\sqrt{|\zeta_i|}}, \quad \bar{\mathcal{I}}_1(\zeta_i) = 0, \quad (4.14)$$

$$\left\{ \begin{array}{l} \bar{\mathcal{J}}_0(\zeta_i) = \mathcal{J}_0(0, -\zeta_i) = \pi \left[(-1) + \frac{(2-i)(3-i)}{2} \cdot \sqrt{\frac{\mathfrak{z}_c^2 - \zeta_i}{|\zeta_i|}} \right] \\ \bar{\mathcal{J}}_1(\zeta_i) = \mathcal{J}_1(0, -\zeta_i) = 0 \\ \bar{\mathcal{J}}_2(\zeta_i) = \mathcal{J}_2(0, -\zeta_i) = \pi \left[\left(\frac{1}{2}\mathfrak{z}_c^2 - \zeta_i \right) + \frac{(2-i)(3-i)}{2} \sqrt{|\zeta_i|(\mathfrak{z}_c^2 - \zeta_i)} \right], \end{array} \right. \quad (4.15)$$

$$[\bar{\mathcal{J}}_0^r(\zeta_i), \bar{\mathcal{J}}_1^r(\zeta_i), \bar{\mathcal{J}}_2^r(\zeta_i)] = [\mathcal{J}_0^r(0, -\zeta_i), \mathcal{J}_1^r(0, -\zeta_i), \mathcal{J}_2^r(0, -\zeta_i)] = \pi \left[-1, 0, \frac{1}{2}\mathfrak{z}_c^2 - \zeta_i \right]. \quad (4.15)_r$$

4.7. Gasdynamic partitions (III). Gasdynamic factorizations (III).

A prefinal form of the sound emergent contribution

Next, the integrals corresponding to the vs -contribution appear, cf. section 4.6, to include a part which is *singular*, concurrently with η^{-1} , with respect to the S -arc (4.1). This circumstance naturally completes the sequence (4.8) of partitions with a last element (the labels r/s mean *regular/singular* with respect to the S -arc):

$$[\tilde{p}_{vs}, \tilde{u}_{vs}, \tilde{v}_{vs}] + [\tilde{p}_{int}, \tilde{u}_{int}, \tilde{v}_{int}] = [\tilde{p}_r, \tilde{u}_r, \tilde{v}_r] + [\tilde{p}_s, \tilde{u}_s, \tilde{v}_s]. \quad (4.16)$$

Now, we carry and re-arrange the calculations 4.6 into the last partition of the sequence (4.16). In Dinu [3] it is noticed that, incidentally and remarkably, to the terms of the mentioned last partition in (4.16) a set of *other four gasdynamic factorizations*, compatible with (4.7), can be naturally associated [via (3.5)]:

$$\begin{aligned} & \mathcal{E}_1^p(\zeta_i)[2(\mathfrak{z}_c^2 - \zeta_i)x\xi + 2\mathfrak{z}_c\sqrt{\mathfrak{z}_c^2 - \zeta_i}t\xi - \sqrt{\mathfrak{z}_c^2 - \zeta_i}y(\xi^2 + \eta^2 + \zeta_i)] \\ & \quad + \mathcal{E}_2^p(\zeta_i)[-2\mathfrak{z}_ct\xi + y(\xi^2 + \eta^2 + \zeta_i) - 2\sqrt{\mathfrak{z}_c^2 - \zeta_i}x\xi] \\ & = [\sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^p(\zeta_i) - \mathcal{E}_2^p(\zeta_i)][2\sqrt{\mathfrak{z}_c^2 - \zeta_i}x\xi + 2\mathfrak{z}_ct\xi - y(\xi^2 + \eta^2 + \zeta_i)] \\ & = [\sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^p(\zeta_i) - \mathcal{E}_2^p(\zeta_i)] \left\{ [y/(x^2 + y^2)][(\mathfrak{z}_ct + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \right\} \end{aligned}$$

$$\begin{aligned} & \sqrt{\mathfrak{z}_c^2 - \zeta_i}t[\mathfrak{z}_c^2(t^2 - x^2) - \zeta_i(x^2 + y^2)] \pm \mathfrak{z}_cx[\mathfrak{z}_c^2(t^2 - x^2) - \zeta_i(2t^2 - x^2 - y^2)] \\ & \quad \equiv (t\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mp x\mathfrak{z}_c)[(\mathfrak{z}_ct \pm x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \end{aligned}$$

$$\begin{aligned} & - \{2\xi\zeta_i\mathcal{T}_1^v(\zeta_i) + (\xi^2 + \eta^2 + \zeta_i)\mathcal{T}_2^v(\zeta_i)\} \\ & \quad + \sqrt{\mathfrak{z}_c^2 - \zeta_i} \cdot \{2\xi\zeta_i[-y\mathcal{E}_1^v(\zeta_i)] + (\xi^2 + \eta^2 + \zeta_i)[\mathfrak{z}_ct\mathcal{E}_1^v(\zeta_i) - x\mathcal{E}_2^v(\zeta_i)]\} \\ & = -[\mathcal{E}_2^v(\zeta_i) - \mathcal{E}_1^v(\zeta_i)\sqrt{\mathfrak{z}_c^2 - \zeta_i}][(\xi^2 + \eta^2 + \zeta_i)(\mathfrak{z}_ct + x\sqrt{\mathfrak{z}_c^2 - \zeta_i}) - 2\zeta_i y\xi] \\ & = -[\mathcal{E}_2^v(\zeta_i) - \mathcal{E}_1^v(\zeta_i)\sqrt{\mathfrak{z}_c^2 - \zeta_i}][1/(x^2 + y^2)](\mathfrak{z}_ct - x\sqrt{\mathfrak{z}_c^2 - \zeta_i})[(\mathfrak{z}_ct + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \end{aligned}$$

$$\begin{aligned} & \mathfrak{z}_c[\mathfrak{z}_c^2(t^4 - t^2x^2 - t^2y^2 - x^2y^2) - \zeta_i(t^2y^2 - x^2y^2 - y^4 - t^2x^2)] \\ & \quad \pm \sqrt{\mathfrak{z}_c^2 - \zeta_i}tx[\mathfrak{z}_c^2(t^2 - y^2) - (\mathfrak{z}_c^2 - \zeta_i)(x^2 + y^2)] \\ & = [t(\mathfrak{z}_ct \mp x\sqrt{\mathfrak{z}_c^2 - \zeta_i}) - \mathfrak{z}_c^2y^2][(\mathfrak{z}_ct \pm x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \end{aligned}$$

where

$$\begin{aligned} \mathcal{E}_1^p(\zeta_i) & \stackrel{\text{def}}{=} MQ_2(\zeta_i) + \mathfrak{z}_cQ_3(\zeta_i), \quad \mathcal{E}_2^p(\zeta_i) \stackrel{\text{def}}{=} \mathfrak{z}_cQ_2(\zeta_i) + M(\mathfrak{z}_c^2 - \zeta_i)Q_3(\zeta_i) \\ \mathcal{E}_1^v(\zeta_i) & \stackrel{\text{def}}{=} Q_3(\zeta_i), \quad \mathcal{E}_2^v(\zeta_i) \stackrel{\text{def}}{=} Q_2(\zeta_i) \\ \mathcal{T}_1^v(\zeta_i) & \stackrel{\text{def}}{=} -y\mathcal{E}_2^v(\zeta_i), \quad \mathcal{T}_2^v(\zeta_i) \stackrel{\text{def}}{=} -x(\mathfrak{z}_c^2 - \zeta_i)\mathcal{E}_1^v(\zeta_i) + t\mathfrak{z}_c\mathcal{E}_2^v(\zeta_i). \end{aligned}$$

We have to notice here that an *analogue* of the first of these factorizations holds true if $\mathcal{E}_1^p, \mathcal{E}_2^p$ are replaced by $\mathcal{E}_1^u, \mathcal{E}_2^u$ corresponding respectively to the u -component of the sound contribution in the interaction solution.

Finally, we naturally get for the sound emergent contribution a more suggestive (prefinal) form (see Dinu [3] for the calculation details):

$$\tilde{p}_r(x, y, t) = \frac{\pi y}{2(x^2 + y^2)^2} \sum_{i=1}^4 \frac{(2-i)(3-i)\sqrt{|\zeta_i|} \tilde{k}_i(\zeta)}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2 \zeta_i} [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^p(\zeta_i) - \mathcal{E}_2^p(\zeta_i)] \cdot [(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \quad (4.17)_p$$

$$\tilde{v}_r(x, y, t) = -\frac{\pi y}{2(x^2 + y^2)^2} \sum_{i=1}^4 \frac{(2-i)(3-i)\sqrt{|\zeta_i|} \tilde{k}_i(\zeta)}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2 \zeta_i} [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^u(\zeta_i) - \mathcal{E}_2^u(\zeta_i)] \cdot [(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \quad (4.17)_u$$

$$\tilde{v}_r(x, y, t) = \frac{\pi\sqrt{1-M^2}}{2(x^2 + y^2)^2} \sum_{i=1}^4 \frac{(2-i)(3-i)\sqrt{|\zeta_i|} \tilde{k}_i(\zeta)}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2 \zeta_i} [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^v(\zeta_i) - \mathcal{E}_2^v(\zeta_i)] \cdot (\mathfrak{z}_c t - x\sqrt{\mathfrak{z}_c^2 - \zeta_i}) [(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \quad (4.17)_v$$

$$\tilde{p}_s(x, y, t) = -\frac{y}{\sqrt{t^2 - x^2 - y^2}} \cdot \frac{\pi}{(x^2 + y^2)^2} \sum_{i=1}^4 \frac{\tilde{k}_i(\zeta)}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2 \zeta_i} \cdot \{ [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^p(\zeta_i) - \mathcal{E}_2^p(\zeta_i)] (t\sqrt{\mathfrak{z}_c^2 - \zeta_i} - \mathfrak{z}_c x) [(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] + [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^p(\zeta_i) + \mathcal{E}_2^p(\zeta_i)] (t\sqrt{\mathfrak{z}_c^2 - \zeta_i} + \mathfrak{z}_c x) [(\mathfrak{z}_c t - x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \} \quad (4.18)_p$$

$$\tilde{u}_s(x, y, t) = \frac{y}{\sqrt{t^2 - x^2 - y^2}} \cdot \frac{\pi}{(x^2 + y^2)^2} \sum_{i=1}^4 \frac{\tilde{k}_i(\zeta)}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2 \zeta_i} \cdot \{ [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^u(\zeta_i) - \mathcal{E}_2^u(\zeta_i)] (t\sqrt{\mathfrak{z}_c^2 - \zeta_i} - \mathfrak{z}_c x) [(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] + [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^u(\zeta_i) + \mathcal{E}_2^u(\zeta_i)] (t\sqrt{\mathfrak{z}_c^2 - \zeta_i} + \mathfrak{z}_c x) [(\mathfrak{z}_c t - x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \} \quad (4.18)_u$$

$$\tilde{v}_s(x, y, t) = -\frac{1}{\sqrt{t^2 - x^2 - y^2}} \cdot \frac{\pi\sqrt{1-M^2}}{(x^2 + y^2)^2} \sum_{i=1}^4 \frac{\tilde{k}_i(\zeta)}{(\xi^2 + \eta^2 + \zeta_i)^2 - 4\xi^2 \zeta_i} \cdot \frac{\zeta_i}{\sqrt{\mathfrak{z}_c^2 - \zeta_i}} \cdot \{ [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^v(\zeta_i) - \mathcal{E}_2^v(\zeta_i)] [t(\mathfrak{z}_c t - x\sqrt{\mathfrak{z}_c^2 - \zeta_i}) - \mathfrak{z}_c y^2] [(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] - [\sqrt{\mathfrak{z}_c^2 - \zeta_i} \mathcal{E}_1^v(\zeta_i) + \mathcal{E}_2^v(\zeta_i)] [t(\mathfrak{z}_c t + x\sqrt{\mathfrak{z}_c^2 - \zeta_i}) - \mathfrak{z}_c y^2] [(\mathfrak{z}_c t - x\sqrt{\mathfrak{z}_c^2 - \zeta_i})^2 - \zeta_i y^2] \} \quad (4.18)_v$$

where

$$\tilde{k}_i(\zeta) = \frac{\tilde{\varepsilon}}{2\pi^2} \cdot \frac{1}{d_{03}^2 \sqrt{1-M^2}} \cdot \frac{Q_1(\zeta_i)}{\prod_{j \neq i} (\zeta_i - \zeta_j)}$$

4.8. A special nature of the gasdynamic context. Inner coherence

It is interesting to remark that to the factorizations mentioned here above [in sections 4.3, 4.5 and 4.7] we have to add the coefficients factorizations and other particular relations included in 4.10. A *special nature* is shown therefore for the gasdynamic context. This special nature is

even more extensive; in fact, we have to notice a *factoring compatibility* ("inner coherence") of the factorizations mentioned here above [see comparatively (4.7) and (4.16), (4.17)].

We have to notice, on the other hand, that the mentioned factorizations may become *immaterial* if the gasdynamic context is extended /lost (see Dinu and Dinu [7]).

4.9. The singular limit of the sound contribution: an optimal explicit form

Next, we take into account the mentioned compatibility (gasdynamic "inner coherence") – precisely: we use (4.7) into (4.17) and (4.18) – to finally get the following *optimal* form of the limit $r_* \rightarrow 0$ of the sound emergent contribution

$$\begin{aligned} & [\tilde{p}_r(\tilde{x}, \tilde{y}, \tilde{t}), \tilde{u}_r(\tilde{x}, \tilde{y}, \tilde{t}), \tilde{v}_r(\tilde{x}, \tilde{y}, \tilde{t})] \\ &= -\overline{K} \sum_{i=1}^4 \frac{k_i^r(\zeta) Q^-(\zeta)}{[\hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)]^2 - \zeta_i \tilde{y}^2} [\hat{k}^-(\zeta)\tilde{y}, -\check{k}^-(\zeta)\tilde{y}, \hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)] \end{aligned} \quad (4.19)$$

$$\begin{aligned} \tilde{p}_s(\tilde{x}, \tilde{y}, \tilde{t}) &= -\frac{\overline{K}}{\sqrt{\tilde{t}^2 - \tilde{x}^2 - \tilde{y}^2}} \cdot H(\tilde{t} - \sqrt{\tilde{x}^2 + \tilde{y}^2}) \\ &\quad \cdot \left\{ \sum_{i=1}^4 \bar{k}_i(\zeta) Q^-(\zeta) \hat{k}^-(\zeta) \frac{\tilde{y}[\hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)]}{[\hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)]^2 - \zeta_i \tilde{y}^2} \right. \\ &\quad \left. + \sum_{i=1}^4 \bar{k}_i(\zeta) Q^+(\zeta) \hat{k}^+(\zeta) \frac{\tilde{y}[\hat{t}\hat{k}^+(\zeta) + \tilde{x}\check{k}^+(\zeta)]}{[\hat{t}\hat{k}^+(\zeta) + \tilde{x}\check{k}^+(\zeta)]^2 - \zeta_i \tilde{y}^2} \right\} \end{aligned} \quad (4.20)_p$$

$$\begin{aligned} \tilde{u}_s(\tilde{x}, \tilde{y}, \tilde{t}) &= \frac{\overline{K}}{\sqrt{\tilde{t}^2 - \tilde{x}^2 - \tilde{y}^2}} \cdot H(\tilde{t} - \sqrt{\tilde{x}^2 + \tilde{y}^2}) \\ &\quad \cdot \left\{ \sum_{i=1}^4 \bar{k}_i(\zeta) Q^-(\zeta) \check{k}^-(\zeta) \frac{\tilde{y}[\hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)]}{[\hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)]^2 - \zeta_i \tilde{y}^2} \right. \\ &\quad \left. + \sum_{i=1}^4 \bar{k}_i(\zeta) Q^+(\zeta) \check{k}^+(\zeta) \frac{\tilde{y}[\hat{t}\hat{k}^+(\zeta) + \tilde{x}\check{k}^+(\zeta)]}{[\hat{t}\hat{k}^+(\zeta) + \tilde{x}\check{k}^+(\zeta)]^2 - \zeta_i \tilde{y}^2} \right\} \end{aligned} \quad (4.20)_u$$

$$\begin{aligned} \tilde{v}_s(\tilde{x}, \tilde{y}, \tilde{t}) &= -\frac{\overline{K}}{\sqrt{\tilde{t}^2 - \tilde{x}^2 - \tilde{y}^2}} \cdot H(\tilde{t} - \sqrt{\tilde{x}^2 + \tilde{y}^2}) \\ &\quad \cdot \left\{ \sum_{i=1}^4 \bar{k}_i(\zeta) Q^-(\zeta) \overset{\circ}{k}(\zeta) \frac{(\tilde{t} + M\tilde{x})[\hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)] - \overline{M}\tilde{y}^2}{[\hat{t}\hat{k}^-(\zeta) + \tilde{x}\check{k}^-(\zeta)]^2 - \zeta_i \tilde{y}^2} \right. \\ &\quad \left. + \sum_{i=1}^4 \bar{k}_i(\zeta) Q^+(\zeta) \overset{\circ}{k}(\zeta) \frac{(\tilde{t} + M\tilde{x})[\hat{t}\hat{k}^+(\zeta) + \tilde{x}\check{k}^+(\zeta)] - \overline{M}\tilde{y}^2}{[\hat{t}\hat{k}^+(\zeta) + \tilde{x}\check{k}^+(\zeta)]^2 - \zeta_i \tilde{y}^2} \right\} \end{aligned} \quad (4.20)_v$$

where we denote

$$k_i^r(\zeta) = \frac{(2-i)(3-i)}{2} \bar{k}_i(\zeta) \sqrt{|\zeta_i|}, \quad \bar{k}_i(\zeta) = \left[\prod_{j \neq i} (\zeta_i - \zeta_j) \right]^{-1}$$

$$\hat{k}^\pm(\zeta_i) = \frac{\mathfrak{z}_c \pm M\sqrt{\mathfrak{z}_c^2 - \zeta_i}}{\sqrt{1 - M^2}}, \quad \check{k}^\pm(\zeta_i) = \frac{M\mathfrak{z}_c \pm \sqrt{\mathfrak{z}_c^2 - \zeta_i}}{\sqrt{1 - M^2}}, \quad \circ k(\zeta_i) = \frac{\zeta_i}{\sqrt{1 - M^2}\sqrt{\mathfrak{z}_c^2 - \zeta_i}}$$

$$Q^\pm(\zeta_i) = Q_1(\zeta_i)[Q_2(\zeta_i) \pm Q_3(\zeta_i)\sqrt{\mathfrak{z}_c^2 - \zeta_i}].$$

4.10. A few useful gasdynamic relations.

We notice at this point a few useful gasdynamic relations:

$$\begin{aligned} \mathfrak{z}_c - M\sqrt{\mathfrak{z}_c^2 + a^2} &= 0 \\ Q_2(-a^2) + Q_3(-a^2)\sqrt{\mathfrak{z}_c^2 + a^2} &= 0 \\ Q_2(b^2) - Q_3(b^2)\sqrt{\mathfrak{z}_c^2 - b^2} &= 0, \quad b^2 < \mathfrak{z}_c^2 \\ Q_2(c^2) - Q_3(c^2)\sqrt{\mathfrak{z}_c^2 - c^2} &= 0, \quad c^2 < \mathfrak{z}_c^2 \end{aligned}$$

$$\begin{aligned} \sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^p(\zeta_i) \pm \mathcal{E}_2^p(\zeta_i) &= (M\sqrt{\mathfrak{z}_c^2 - \zeta_i} \pm \mathfrak{z}_c)[Q_2(\zeta_i) \pm \sqrt{\mathfrak{z}_c^2 - \zeta_i}Q_3(\zeta_i)] \\ \sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^u(\zeta_i) \pm \mathcal{E}_2^u(\zeta_i) &= (\sqrt{\mathfrak{z}_c^2 - \zeta_i} \pm M\mathfrak{z}_c)[Q_2(\zeta_i) \pm \sqrt{\mathfrak{z}_c^2 - \zeta_i}Q_3(\zeta_i)] \\ \sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^v(\zeta_i) \pm \mathcal{E}_2^v(\zeta_i) &= \pm[Q_2(\zeta_i) \pm \sqrt{\mathfrak{z}_c^2 - \zeta_i}Q_3(\zeta_i)] \end{aligned}$$

$$\begin{aligned} \sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^p(\zeta_i) - \mathcal{E}_2^p(\zeta_i) &= 0, \quad 1 \leq i \leq 3 \\ \sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^u(\zeta_i) - \mathcal{E}_2^u(\zeta_i) &= 0, \quad i = 2, 3 \\ \sqrt{\mathfrak{z}_c^2 - \zeta_i}\mathcal{E}_1^v(\zeta_i) - \mathcal{E}_2^v(\zeta_i) &= 0, \quad i = 2, 3 \end{aligned}$$

$$\mathcal{E}_1^p(\zeta_1) = 0, \quad \mathcal{E}_2^p(\zeta_1) = 0$$

to get that

$$k_2^r(\zeta) = 0, \quad k_3^r(\zeta) = 0; \quad \hat{k}^-(\zeta_1) = 0; \quad Q^+(\zeta_1) = 0, \quad Q^-(\zeta_2) = 0, \quad Q^-(\zeta_3) = 0$$

in the coefficients of (4.19), (4.20) – thus annulling some of these coefficients.

4.11. Final notes

This sound contribution corresponds to the incidence [obtained from (3.2) in the limit $r_* \rightarrow 0$]

$$[\tilde{u}(\tilde{x}, \tilde{y}), \tilde{v}(\tilde{x}, \tilde{y})] = \frac{\tilde{\varepsilon}}{2\pi} \cdot \frac{[-\tilde{y}, \tilde{x}]}{\tilde{x}^2 + \tilde{y}^2}, \quad \tilde{s} \equiv \tilde{p} \equiv 0; \quad (\tilde{x}, \tilde{y}) \neq (0, 0). \quad (4.21)$$

We have to complete these results with the explicit form of the rest of the limit $r_* \rightarrow 0$ of the Ribner solution by carrying (4.19), (4.20) and (4.21) into (3.8)–(3.11).

It is easy to show, finally, that the singular structure of the cumulative contribution of (4.19) and (4.20) consists in the sound singularities continuously distributed along the \mathcal{S} -arc and is completed with a vorticity singularity laid at the point $(\tilde{x} = 0, \tilde{y} = 0)$. The other singularities of (4.19), (4.20) are proven to be pseudosingularities: they appear to be *compensated* in the sums $\tilde{p}_r + \tilde{p}_s$, $\tilde{u}_r + \tilde{u}_s$, $\tilde{v}_r + \tilde{v}_s$. In fact this result is suggested by Figure 1.

The presence, at $\tilde{t} > 0$, of the \mathcal{S} -arc – which supports a continuous distribution of sound

singularities – could be regarded as a *widening*, corresponding to a nonlinear subconscious, of an incident vorticity singularity.

We end this section by noticing the *irreversible* character of this solution.

5. AN OBLIQUE EXTENSION OF RIBNER'S PARALLEL SOLUTION

5.1. Details of the oblique extension

We tentatively present the sound part (4.19), (4.20) of the parallel interaction solution in the form

$$\begin{cases} \tilde{p}_r + \tilde{p}_s & \equiv \tilde{p}_{||}(x, y, t; \zeta_1, \zeta_2, \zeta_3, \zeta_4; \mathfrak{z}_c; Q_1, Q_2, Q_3) \\ \tilde{u}_r + \tilde{u}_s & \equiv \tilde{u}_{||}(x, y, t; \zeta_1, \zeta_2, \zeta_3, \zeta_4; \mathfrak{z}_c; Q_1, Q_2, Q_3) \\ \tilde{v}_r + \tilde{v}_s & \equiv \tilde{v}_{||}(x, y, t; \zeta_1, \zeta_2, \zeta_3, \zeta_4; \mathfrak{z}_c; Q_1, Q_2, Q_3) \end{cases} \quad (5.1)$$

which has a “*Lorentz type*” arguments structure [the arguments structure (5.1) could be regarded as being a code (“cipher”) which filters out the passage to an oblique approach]. Incidentally, this form appears to be *extensible* to the case of oblique interactions. The nature of the extension is suggested in Figure 2.

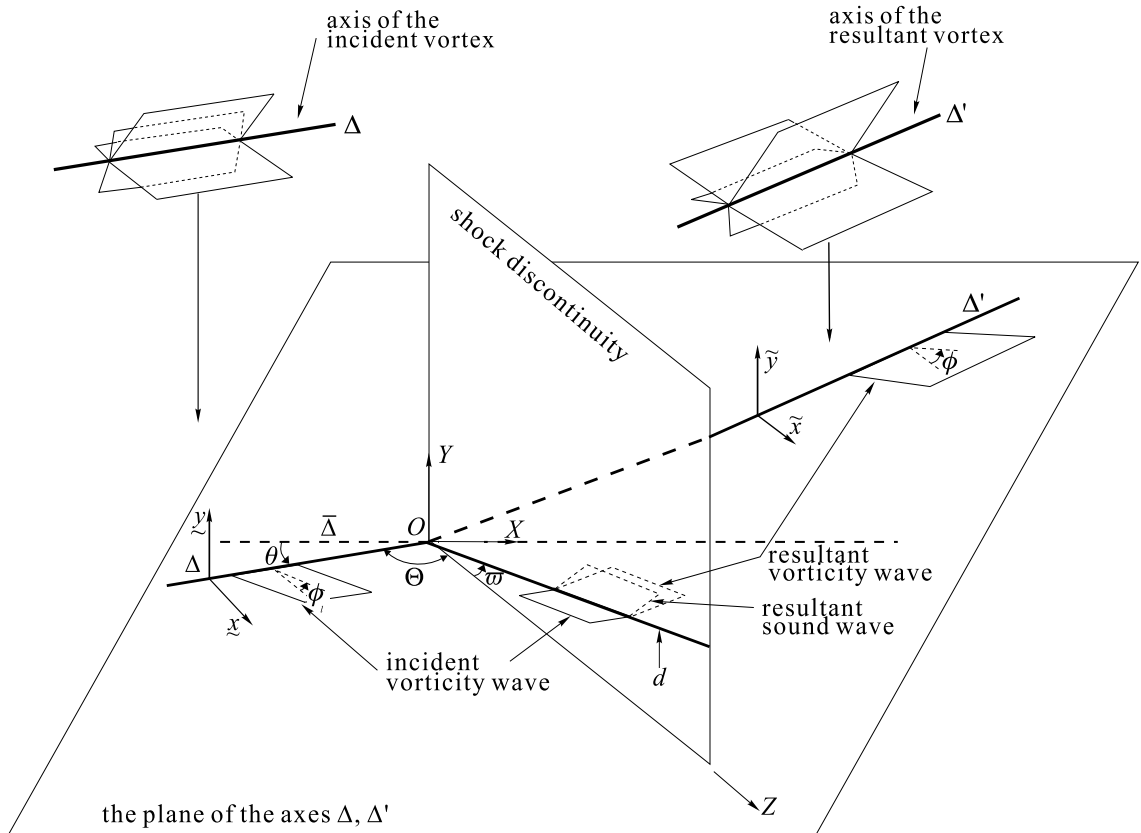


FIGURE 2 Details of the oblique construction

Let Δ be the axis of the (oblique) incident vortex and let θ be the angle between this axis and the axis $\overline{\Delta}$ [along which a sense is indicated by the coordinate X]. In Figure 2 we particularly depict the passage of a plane of zero phase corresponding to a certain incident monochromatic vorticity wave in the Fourier representation [analogous to (3.3)] of the incident vortex; let d be the intersection of this plane with the shock plane. We denote by ϖ the angle between the line d and the axis OZ . Let $\pi(d_1, d_2)$ the plane spanned by two concurrent lines d_1, d_2 . We use the facts of Figure 1 in order to characterize the refraction of the plane $\pi(d, \Delta)$. To complete the Fourier–Snell representation of the considered passage we need the expression of the dihedral angle $\overline{\phi}_l$ of the planes $\pi(d, \Delta)$ and $\pi(d, \overline{\Delta})$ in terms of the angles θ and ϖ . We have

$$\cot \overline{\phi}_l = -\frac{\sqrt{1 + \tan^2 \varpi}}{\tan \theta \tan \varpi} \stackrel{\text{def}}{=} -\overline{\beta}; \quad -\frac{\pi}{2} \leq \theta \leq \frac{\pi}{2}. \quad (5.2)$$

We adapt the Figure 1 to the analysis around the line d by using a bar over the notations of Figure 1. So, ϕ_l, ϕ, ϕ' of the Figure 1 become $\overline{\phi}_l, \overline{\phi}, \overline{\phi}'$ around the line d . The same as in the parallel case, it is easy to be seen that the envelope of the refracted zero-phase vorticity planes, which result from the passage of the mentioned incident vortex, is a straightline Δ' – the axis of the refracted vorticity (Figure 2). A straightforward geometrical analysis shows that, $\tan \theta' = \frac{M}{M'} \tan \theta$ – where θ' is the angle between the axes Δ' and $\overline{\Delta}$.

Now, the parallel solution or its oblique extensions concern an interaction element - which models the passage through the discontinuity of a *single* incident vortex. To an oblique interaction element we should associate the oblique extensions $\underline{x}, \underline{y}, \underline{z}$ and, respectively, $\tilde{x}, \tilde{y}, \tilde{z}$ of the Lagrange parallel frames (3.1) [Figure 2]. These frames [as well as the frame X, Y, Z] depend on the interaction element considered. In fact: the axis OZ results from the intersection between the plane $\pi(\Delta, \overline{\Delta})$ and the plane of the shock discontinuity.

In section 5.4 the passages of some vortices of distinct and [cf. section 5.2] significant inclinations are compared.

The direction \underline{z} of the frame $\underline{x}, \underline{y}, \underline{z}$ is laid along the axis Δ of the oblique vortex; therefore the oblique incident vortex has again the form (3.2) in this frame.

The direction \tilde{z} of the frame $\tilde{x}, \tilde{y}, \tilde{z}$ will be placed along the axis Δ' of the resulting vorticity; the emergent sound field will get in the frame $\tilde{x}, \tilde{y}, \tilde{z}$ the structure $\tilde{p}, \tilde{u}, \tilde{v}, \tilde{w}$.

In order to pass from the frame $\underline{x}, \underline{y}, \underline{z}$ to the frame $\tilde{x}, \tilde{y}, \tilde{z}$ we use an intermediate frame $\hat{X}, \hat{Y}, \hat{Z}$ – an analogue of the frame \hat{X}, \hat{Y} of Figure 1. The origins Q [of the frame $\underline{x}, \underline{y}, \underline{z}$] and \hat{O} [of the frame $\hat{X}, \hat{Y}, \hat{Z}$] coincide at the initial time $\tilde{t} = 0$.

5.2. Subcritical and supercritical inclinations.

Remark 5.1. We put $\Theta = \frac{\pi}{2} - \theta \text{sign} \theta$ and notice that the requirement

$$|\overline{\beta}| \leq \beta_c \quad (5.3)$$

consists, cf. (5.2), in

$$1 \leq \frac{\sqrt{1 + \tan^2 \varpi}}{|\tan \varpi|} \leq \frac{\beta_c}{\tan \Theta}$$

or, *equivalently*, in

$$\tan \Theta \leq \beta_c \quad (5.4)$$

together with

$$|\tan \varpi| \geq \frac{\tan \Theta}{\sqrt{\beta_c^2 - \tan^2 \Theta}}. \quad (5.5)$$

This suggests that we ought to distinguish between the *supercritical* and *subcritical* inclinations of the incident vortex axis respectively characterized by $\tan \Theta \geq \mathfrak{z}_c$ and $\tan \Theta \leq \mathfrak{z}_c$. In fact, for a supercritical inclination of the mentioned axis the possibility (5.3) is excluded cf. (5.4) and we must require $|\mathfrak{z}| \geq \mathfrak{z}_c$, so that the sound component of the refracted solution is entirely *pseudoelliptic*. On the other hand, for a subcritical inclination of the mentioned axis a pseudohyperbolic part, isolated by the requirement (5.5), is allowed in a *mixed type* sound component of the refracted solution. \square

5.3. Extended Lorentz coordinates. The subcritical case.

Let us consider next the case of *subcritical* incident vortices (see Dinu and Dinu [5] for the details of the supercritical case). This case is largely similar, to the (subcritical) case considered (for $\Theta = 0$) in §4. It is easy to show that the zero-phase planes corresponding to the sound component of the emergent solution envelop a circular *sonic cone* with the axis Δ' and the vertex angle 2χ where

$$\sin \chi = \frac{1}{M} \cos \theta' = \frac{\cos \theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \cos^2 \theta}}$$

and we notice that for a real χ we must require $\tan \Theta \leq \mathfrak{z}_c$, i.e. subcriticality.

In the sequel we parallel (3.5) by introducing the *extended Lorentz coordinates*

$$\left\{ \begin{array}{l} x = \frac{\mathfrak{z}_c \cos \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \tilde{x} + \frac{M \mathfrak{z}_c}{M} \tilde{t} + \frac{M \mathfrak{z}_c}{M} \cdot \frac{(\text{sign } \theta) \sin \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \tilde{z} = \frac{X}{\sqrt{1 - M^2}}; \\ y = \tilde{y}; \quad z = \tilde{z} \\ t = \frac{M \mathfrak{z}_c^*(\Theta) \cos \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \tilde{x} + \frac{\mathfrak{z}_c^2}{M \mathfrak{z}_c^*(\Theta)} \tilde{t} + \frac{\mathfrak{z}_c^2}{M \mathfrak{z}_c^*(\Theta)} \cdot \frac{(\text{sign } \theta) \sin \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \tilde{z} \end{array} \right. \quad (5.7)$$

where

$$\mathfrak{z}_c^*(\Theta) \stackrel{\text{def}}{=} \sqrt{\mathfrak{z}_c^2 - \tan^2 \Theta}, \quad \mathfrak{z}^* = \frac{\mathfrak{z}}{\cos \Theta},$$

and notice that

$$t^2 - x^2 - y^2 = \left[\tilde{z} + (\text{sign } \theta) \frac{\tilde{t}}{\sin \chi} \right]^2 \tan^2 \chi - (\tilde{x}^2 + \tilde{y}^2).$$

5.4. The simplest nonstatistical model of turbulence refraction and its relation with Lighthill's model.

The explicit form of the sound emergent contribution in the limit $r_* \rightarrow 0$ of the mentioned subcritical interaction is

$$\begin{aligned} \tilde{p}(x, y, t) &= \{1 + [\mathfrak{z}_c^*(\Theta) - \mathfrak{z}_c]\} \\ &\quad \cdot \tilde{p}_{\parallel}[x, y, t; a^{*2}, \varepsilon_b b^{*2}, \varepsilon_c c^{*2}, v^{*2}; \mathfrak{z}_c^*(\Theta); Q_1^*, Q_2^*, Q_3^*] \\ &\quad + M[\mathfrak{z}_c^*(\Theta) - \mathfrak{z}_c] \\ &\quad \cdot \tilde{u}_{\parallel}[x, y, t; a^{*2}, \varepsilon_b b^{*2}, \varepsilon_c c^{*2}, v^{*2}; \mathfrak{z}_c^*(\Theta); Q_1^*, Q_2^*, Q_3^*] \end{aligned}$$

$$\begin{aligned}
\tilde{u}(x, y, t) &= \overline{M} \left\{ 1 + \frac{M^2}{\overline{M}^2} \mathfrak{z}_c \left[\mathfrak{z}_c^*(\Theta) - \mathfrak{z}_c - \frac{1}{\mathfrak{z}_c} \tan^2 \Theta \right] \right\} \cdot \frac{\cos \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \\
&\quad \cdot \tilde{u}_{\parallel}[x, y, t; a^{*2}, \varepsilon_b b^{*2}, \varepsilon_c c^{*2}, v^{*2}; \mathfrak{z}_c^*(\Theta); Q_1^*, Q_2^*, Q_3^*] \\
&+ \frac{M}{\overline{M}} \mathfrak{z}_c \left[\mathfrak{z}_c^*(\Theta) - \mathfrak{z}_c - \frac{1}{\mathfrak{z}_c} \tan^2 \Theta \right] \cdot \frac{\cos \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \\
&\quad \cdot \tilde{p}_{\parallel}[x, y, t; a^{*2}, \varepsilon_b b^{*2}, \varepsilon_c c^{*2}, v^{*2}; \mathfrak{z}_c^*(\Theta); Q_1^*, Q_2^*, Q_3^*] \\
\tilde{v}(x, y, t) &= \tilde{v}_{\parallel}[x, y, t; a^{*2}, \varepsilon_b b^{*2}, \varepsilon_c c^{*2}, v^{*2}; \mathfrak{z}_c^*(\Theta); Q_1^*, Q_2^*, Q_3^*] \\
\tilde{w}(x, y, t) &= M \left\{ 2 + \frac{M^2}{\overline{M}^2} \mathfrak{z}_c [\mathfrak{z}_c^*(\Theta) - \mathfrak{z}_c] \right\} \cdot \frac{(\text{sign } \theta) \sin \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \\
&\quad \cdot \tilde{u}_{\parallel}[x, y, t; a^{*2}, \varepsilon_b b^{*2}, \varepsilon_c c^{*2}, v^{*2}; \mathfrak{z}_c^*(\Theta); Q_1^*, Q_2^*, Q_3^*] \\
&+ \left\{ 1 + \frac{M^2}{\overline{M}^2} \mathfrak{z}_c [\mathfrak{z}_c^*(\Theta) - \mathfrak{z}_c] \right\} \cdot \frac{(\text{sign } \theta) \sin \Theta}{\sqrt{\overline{M}^2 + (M^2 - \overline{M}^2) \sin^2 \Theta}} \\
&\quad \cdot \tilde{p}_{\parallel}[x, y, t; a^{*2}, \varepsilon_b b^{*2}, \varepsilon_c c^{*2}, v^{*2}; \mathfrak{z}_c^*(\Theta); Q_1^*, Q_2^*, Q_3^*]
\end{aligned}$$

where x, y, t depend on $\tilde{x}, \tilde{y}, \tilde{z}, \tilde{t}$ cf. (5.7) and we denote

$$\begin{cases} a^{*2} = a^2 + \tan^2 \Theta, & b^{*2} = |b^2 - \tan^2 \Theta|, & c^{*2} = |c^2 - \tan^2 \Theta|, & v^{*2} = 1 + \tan^2 \Theta \\ \varepsilon_b = \text{sign}(\tan^2 \Theta - b^2), & \varepsilon_c = \text{sign}(\tan^2 \Theta - c^2) \end{cases}$$

$$\begin{cases} Q_1^*(\mathfrak{z}^{*2}) \stackrel{\text{def}}{=} d_{11} \mathfrak{z}^{*2} + (d_{11} \tan^2 \Theta + d_{12}) \equiv Q_1(\bar{\mathfrak{z}}^2) \\ Q_2^*(\mathfrak{z}^{*2}) \stackrel{\text{def}}{=} d_{01} \mathfrak{z}^{*2} + (d_{01} \tan^2 \Theta + d_{02}) \equiv Q_2(\bar{\mathfrak{z}}^2) \\ Q_3^*(\mathfrak{z}^{*2}) \stackrel{\text{def}}{=} d_{03} \mathfrak{z}^{*2} + (d_{03} \tan^2 \Theta + d_{04}) \equiv Q_3(\bar{\mathfrak{z}}^2). \end{cases}$$

A suggestive description concerning the refraction of a turbulence model through a shock discontinuity is considered in Figure 3. This description brings together and compares the passage through the discontinuity of an incident point vortex the axis of which is parallel to the shock and the passage through the same shock of a point vortex the axis of which is oblique – subcritical or supercritical.

In the singular limit of the interaction solution [see section 4.4] the *subcritical* contribution and the *supercritical* one – which appear to be essentially and exhaustively included – are distinguished by differences of a “relativistic” nature. Precisely: in the singular limit of the interaction solution the emergent sound is *singular* in the subcritical contribution and it is *regular* in the supercritical contribution (see Figure 3).

In Dinu and Dinu [6] it is shown that the “relativistic” discontinuity in the nature of the emergent sound, corresponding to the singular limit of the interaction solution, appears to be dissembled (hidden) in the re-weighted interaction solution.

In the Lighthill’s fundamental paper [14] the turbulence is acoustically modelled by a distribution of quadrupoles – which is equivalent with a “weighted” distribution of point vortices.

We notice that the *explicit* character of Figure 3 induces an *exhaustive* nonstatistical classification into Lighthill’s *implicit* description.

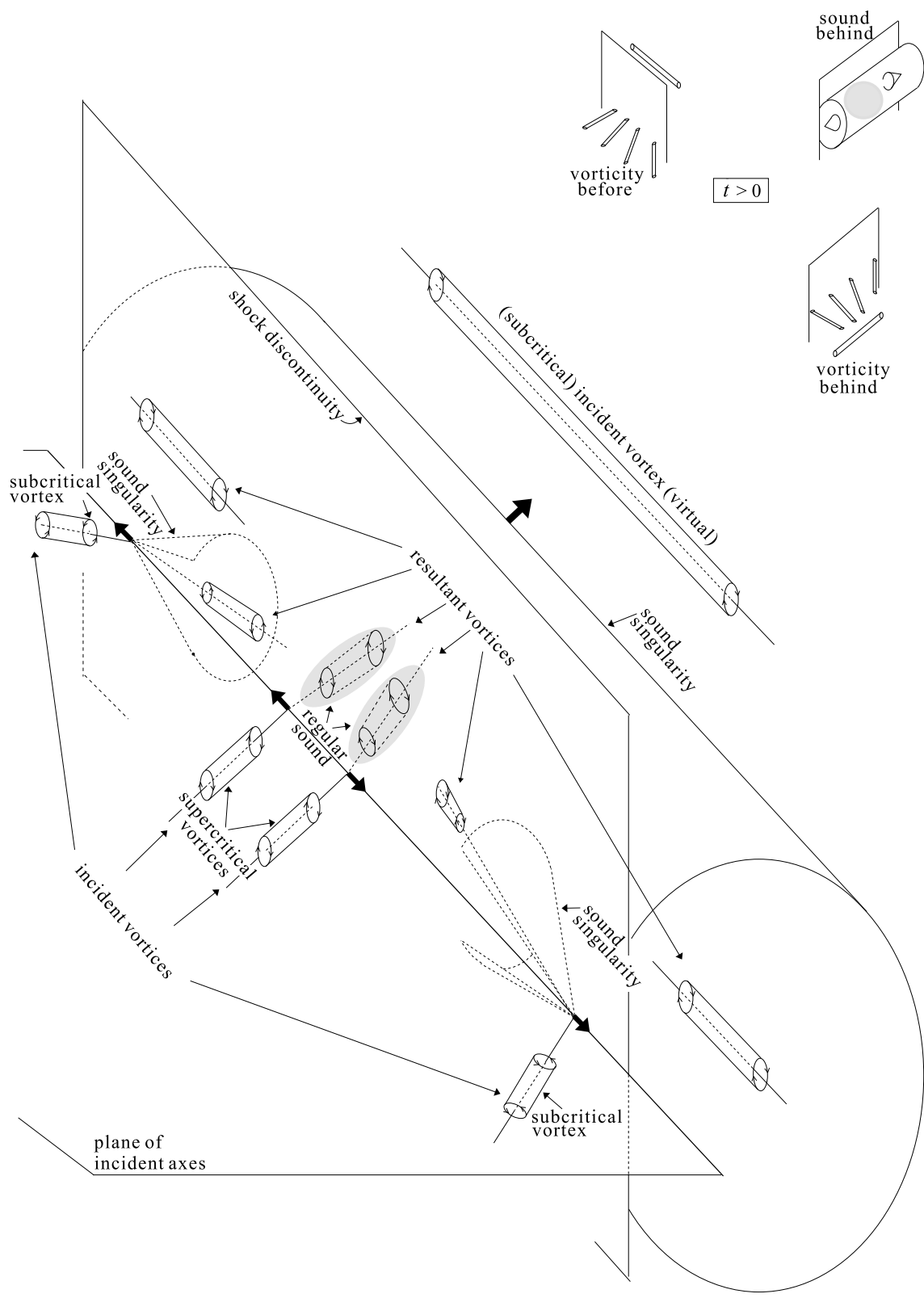


FIGURE 3 The simplest nonstatistical model of turbulence refraction ($\bar{t} > 0$)

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