

Reshaping nemato-elastic sheets

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Abstract. We consider three-dimensional reshaping of thin nemato-elastic sheets containing half-charged defects upon nematic-isotropic transition. Gaussian curvature, that can be evaluated analytically when the nematic texture is known, differs from zero in the entire domain and has a dipole or hexapole singularity, respectively, at defects of positive or negative sign. The latter kind of defects appears in not simply connected domains. Three-dimensional shapes dependent on boundary anchoring are obtained with the help of finite element computations.

1 Introduction

Liquid crystal elastomers and glasses [1], made of cross-linked polymeric chains with embedded mesogenic structures, combine orientational properties of liquid crystals with shear strength of solids, and were envisaged by de Gennes as prototype artificial muscles [2]. Their specific feature is a strong coupling between the director orientation and mechanical deformations, which can be controlled by the various physical and chemical agents. When the material undergoes a phase transition from the isotropic to nematic state, it strongly elongates along the director and, accordingly, shrinks in the normal direction to preserve its volume; the opposite effect takes place as a result of the reverse transition. Stresses arising due to these intrinsic deformations were investigated for flat sheets where they were shown to lead to phase separation of isotropic and nematic domains [3] or formation of persistent defects that are not necessitated by topology [4].

Internal stresses can be relaxed when three-dimensional (3D) deformations are allowed. The reshaping effect causes bending of flat thin sheets into curved shells. Aharoni *et al.* [5] studied the various nematic textures that can be impressed in the material to induce a desired two-dimensional (2D) metric that would determine a 3D shape upon transition from nematic to isotropic state (NIT). This opens the way to construct surfaces with non-zero Gaussian curvature out of flat sheets with no stretching [6], or, more generally, to change the Gaussian curvature of shells. While the Gaussian curvature is an intrinsic property that can be computed based a surface metric only [7], computing an actual 3D shape is a far more challenging task, which is additionally complicated by constraints on nematic tissues imposed by boundary

conditions or topology of closed manifolds that necessitate emergence of defects.

A 3D shape can be computed analytically only for a symmetric texture, and the only available example is deformation of a circle containing a defect with unit circulation into a cone or an anticone [6,8]. This case is exceptional in two respects. First, the natural nematic texture induced within a circle by either tangential or normal boundary anchoring contains two half-charged defects which have a lower energy than a single defect of unit charge. Second, the Gaussian curvature induced by a unit charge defect vanishes everywhere except the vicinity of the defect itself [5], where it can be regularised either by local stretching [6] or by depletion of nematic order [8]. Away from the defect, where the Gaussian curvature vanishes, folding may help to accommodate an extended perimeter of the circle into a sphere with a shrinking radius [8], in a way similar to crumpling of isotropic non-extensible sheets [9].

In a more difficult and realistic case of half-charged defects, even planar textures can be computed analytically only in simplest configurations, and the lack of axial symmetry leaves little hope for analytical theory of 3D shapes. The Gaussian curvature differs then from zero also outside defect cores, which is conducive to smooth 3D shapes. In this paper, we compute numerically the shapes generated upon NIT from naturally formed nematic textures. We first summarise our basic methods: analytical, starting with metric transformation induced by NIT and extending, in the case when the nematic texture is known, to computation of Gaussian curvature, and numerical, indispensable for visualising actual 3D shapes. We consider next representative particular cases: a vicinity of isolated defects, where the induced structure can be well resolved; an elliptic sheet containing two half-charged defects; and a sheet with two holes where negatively charged defects naturally appear.

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2 Intrinsic and extrinsic properties

2.1 Order parameter and metric transformation

We consider a thin sheet with preferred parallel orientation of the director on both outer surfaces. The material is described then by the 2D nematic order parameter, presented as a traceless symmetric tensor dependent on 2D coordinates:

$$Q^\alpha_\beta = S \left(n^\alpha n_\beta - \frac{1}{2} \delta^\alpha_\beta \right), \quad (1)$$

where n_α are vector components of the director, δ^α_β is the Kronecker delta, and S is the scalar order parameter equal to unity in a perfectly aligned nematic state. In thin elastic sheets, bending is favoured energetically over stretching, as bending rigidity is proportional to the cube of the thickness [10]; therefore in-shell elastic deformations must be negligible. Under this assumption, an infinitesimal interval is transformed [8] as a result of a change \tilde{Q}^α_β of the nematic state as

$$d\xi^\alpha = T^\alpha_\beta dx^\beta, \quad T^\alpha_\beta = N^{-1/2} \left(\delta^\alpha_\beta + a \tilde{Q}^\alpha_\beta \right), \quad (2)$$

where a is a metric factor measuring the relative extension and contraction, and N is a normalisation factor; summation over paired indices is presumed. This is the simplest form suggested by the tensor character of both the metric transformation and the nematic order parameter. The original metric tensor \mathbf{g}^0 is transformed thereby to $\mathbf{g} = \mathbf{T} \mathbf{g}^0 \mathbf{T}$; the transformation can be made area-preserving [8] by choosing N to ensure $\det(\mathbf{T}) = 1$. In the case of transition from nematic ($S = 1$) to isotropic ($S = 0$) state (NIT), the explicit area-preserving metric expression is

$$g_{\alpha\beta} = (1 - a^2)^{-1} [(1 + a^2)g_{\alpha\beta}^0 - 2aQ_{\alpha\beta}]. \quad (3)$$

If the coordinate axes x^α , ξ^α are oriented, respectively, along and normally to the director, eq. (2) simplifies [11] to

$$d\xi^1 = \frac{1}{\ell} dx^1, \quad d\xi^2 = \ell dx^2, \quad \ell = \sqrt{\frac{1+a}{1-a}}, \quad (4)$$

and the transformed metric is diagonal with the elements ℓ^{-2} , ℓ^2 .

The transformed metric can be used to compute *intrinsic* properties of bent sheets or shells but not their *extrinsic* properties defining their position in space. Among the former, the most important one is Gaussian curvature equal to the only non-zero component $K = R_{1212}$ of the Riemann curvature tensor [7]. It is defined by standard formulas dependent on the first and second derivatives of the metric tensor.

2.2 Numerical methods for 3D shapes

Computing actual 3D shapes which, unlike Gaussian curvature, are not determined by intrinsic characteristics of

a surface alone, is a much more difficult task that can be only accomplished numerically. We carried out computations by triangulating the surface and defining the nematic order parameter at the grid nodes. The nematic director on triangular tiles was defined as the average of the three vertices. Normal vectors \mathbf{m}_i were computed for each tile, and the normal vectors at nodes \mathbf{m}_j were defined as the average of the normals at the surrounding tiles. If the nematic field was known analytically, as in some following examples, the nematic director was defined at the centres of triangular tiles.

The numerical procedure was based on minimising the energy functional defined as

$$E = \sum_{\text{edges}} (l_i - l_i^0)^2 + \kappa \sum_{\text{nodes}} \sum_j (1 - \mathbf{m}_i \cdot \mathbf{m}_{ij}). \quad (5)$$

Here, the first term accounts for deviation of the length l_i of an i th edge from the value l_i^0 defined by eq. (2). In the second term, \mathbf{m}_{ij} denotes the normal to the j th tile of those surrounding an i th node. The sum over all neighbours measures the deviation from their average orientation \mathbf{m}_i , which accounts for the curvature of the bent shell. Since bending rigidity is much weaker than in-shell shear modulus, the ratio κ of bending rigidity to in-shell elasticity should be small. In order to speed up numerical algorithm at early stages, it was gradually decreased from 10^{-4} to 5×10^{-6} , which allowed us to arrive as close as possible to the required degree of local extension or shrinkage.

The energy minimisation procedure followed a Monte Carlo (MC) routine, whereby the triangular finite elements were addressed at random, and NIT was imitated by changing the length of their sides (edges) according to eq. (2) and further rescaling to eliminate numerical errors in maintaining the area conservation. The computation continued until the relative energy decrease during a MC cycle was less than 10^{-8} . The average execution time of 1000 MC cycles for a typical triangulated mesh with 1300 nodes and 2500 elements using an Intel core i7 10GB RAM work station was about 3 minutes.

When the nematic texture was not known analytically, we computed it in the one-constant approximation by minimising the nematic energy $\int (\nabla \mathbf{n})^2 d\Sigma$ over a studied domain with appropriate anchoring conditions at boundaries. The derivatives were approximated by differences between the directors at neighbouring nodes. Although the director is more naturally defined on tiles, redefining it on nodes improves numerical accuracy due to a larger number of neighbours (six rather than three). We resolved the defect core structure only in the case of isolated defects leaving otherwise the scalar order parameter S equal to unity, but triangulation density was increased in the vicinity of defects. An amended procedure is applicable to computation of textures on curved surfaces. In this case, covariant derivatives can be computed by virtually rotating neighbouring tiles into a common plane before comparing the directors, and an additional energy penalty is introduced according to the surface curvature along the director. There was, however, no need to implement this

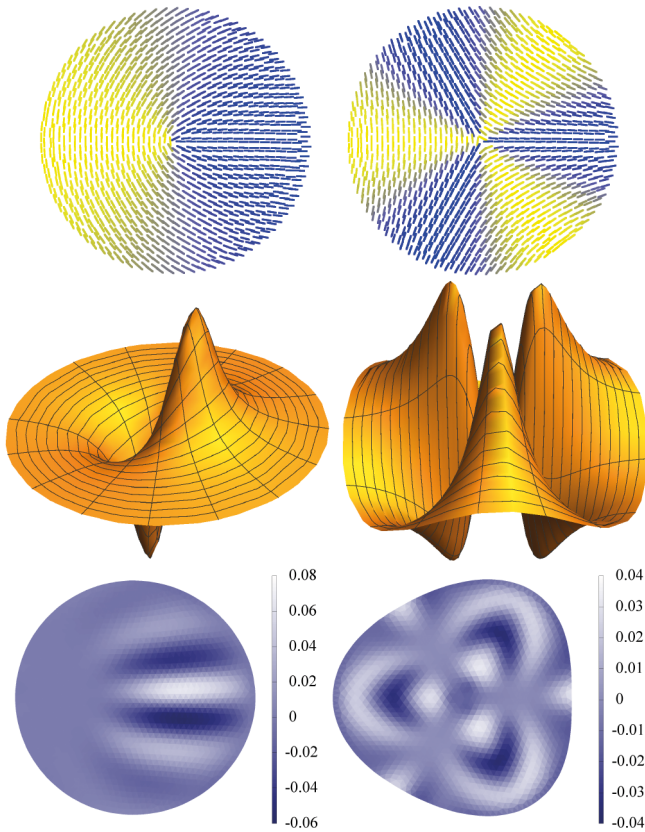


Fig. 1. The vicinity of isolated positive (left) and negative (right) half-charged defects. Upper row: the director field; the shading imitates the view in cross-polarisers. Middle row: the regularised Gaussian curvature. Lower row: shade-coded relief maps of 3D shapes; scale bars show the deviation from the original plane.

procedure here, since we only studied transition from flat nematic sheets to deformed shapes in the isotropic state.

3 From textures to shapes

3.1 Vicinity of defects

Strong reshaping effects in the vicinity of defects are of special interest, and can be studied by considering isolated defects, far removed from other defects and boundaries. The texture in the vicinity of positive and negative half-charged defects has different symmetry (fig. 1), even though the nematic order parameter is expressed in a similar way. In a vicinity of defects of the charge $\pm 1/2$ (but outside their cores) the tensor order parameter is

$$\mathbf{Q} = \frac{1}{2} \begin{pmatrix} \cos \phi & \pm \sin \phi \\ \pm \sin \phi & -\cos \phi \end{pmatrix}, \quad (6)$$

where ϕ is the polar angle. Starting from the Cartesian metric \mathbf{g}^0 , we obtain using eq. (3) the transformed metric

$$\mathbf{g} = \frac{1}{1-a^2} \begin{pmatrix} 1-2a \cos \phi + a^2 & \mp 2a \sin \phi \\ \mp 2a \sin \phi & 1+2a \cos \phi + a^2 \end{pmatrix}. \quad (7)$$

The Gaussian curvature K_{\pm} of a bent shell formed upon NIT is derived from this metric:

$$K_+ = \frac{a \cos \phi}{r^2(1-a^2)}, \quad K_- = -\frac{3a \cos 3\phi}{r^2(1-a^2)}. \quad (8)$$

These simple expressions are in accordance with the symmetry of the bent shell around the defect. The curvature diverges at the defect location ($r \rightarrow 0$) leading to a dipole or hexapole singularity, respectively, for defects of positive or negative sign. For the positive charge, the curvature is positive near the defect's "comet tail" at $\phi = 0$, while a saddle geometry with negative Gaussian curvature is indicated on the opposite side. For the negative charge, there is a threefold symmetry, matching the symmetry of the nematic field (fig. 1).

The divergence can be regularised by taking into account vanishing S at the defect core. For defects of either sign, the radial dependence $S(r)$ is identical to that of the amplitude of a complex scalar field near a defect of *unit* charge [12], and satisfies the equation

$$S''(r) + r^{-1}S'(r) + S(1-r^{-2}-S^2) = 0, \quad (9)$$

where the radial coordinate is scaled by the healing length. The regularised Gaussian curvature within a circle encompassing the defect core is shown in fig. 1. The director fields, curvature plots, and relief maps in fig. 1 are drawn at a higher resolution than in figures depicting entire domains. The symmetry of these forms is universal, although it may be distorted in the vicinity of boundaries.

3.2 Elliptic domain

In only two known examples, a nematic texture containing half-charged defects can be obtained analytically in the one-constant approximation by means of conformal transformation [13]. The simplest case is an ellipse where the director is aligned along coordinate lines $u = \text{const}$ (if it is anchored normal to the boundary) or $v = \text{const}$ (if the anchoring is tangential) of the elliptic coordinate system, which are identical to the isolines of the real and imaginary part of the analytic complex function $w = \sin z$ (fig. 2). Upon NIT, the metric of the resulting curved sheet is readily obtained by modifying the elliptic metric according to eq. (4):

$$\mathbf{g} = g \text{diag}(\ell^{-2}, \ell^2), \quad g = \frac{1}{2}(\cosh 2v - \cos 2u), \quad (10)$$

where the half-focal distance is normalised to unity. This expression is equally applicable to textures with the director along the coordinate lines $u = \text{const}$ or $v = \text{const}$; one needs only to interchange the metric factors corresponding to the two variables. In both cases, the Gaussian curvature is computed as

$$\begin{aligned} K &= \pm \frac{1}{g} \left[\frac{\partial}{\partial u} \left(\frac{1}{g} \frac{\partial g}{\partial u} \right) + \frac{\partial}{\partial v} \left(\frac{1}{g} \frac{\partial g}{\partial v} \right) \right] \\ &= \pm \frac{16a(\cosh 2v \cos 2u - 1)}{(1-a^2)(\cosh 2v - \cos 2u)^2}. \end{aligned} \quad (11)$$

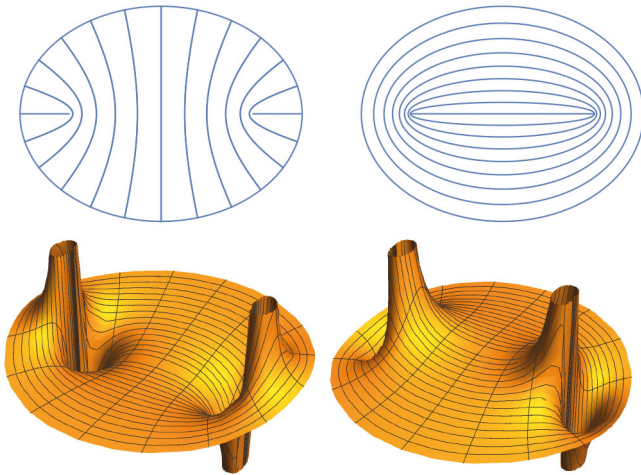


Fig. 2. Above: director orientation for normal (left) and tangential (right) boundary anchoring. Below: Gaussian curvature for the respective cases.

This expression has a dipolar singularity at both foci (see fig. 2). Near the foci at $x = \pm 1$, $y = 0$, one can set $u \approx \pm\sqrt{2r} \sin(\phi/2)$, $v \approx \pm\sqrt{2r} \cos(\phi/2)$ and recover the first formula in (8) in the leading order of expansion in the distance $r \ll 1$ from either focus. The difference is in the position of “comet tails” of both defects, which are directed toward the centre of the ellipse when the anchoring is tangential, and outwards when the anchoring is normal. The positive and negative curvature regions are situated accordingly, so that the Gaussian curvature is positive between the foci and the nearest boundary in the case of normal anchoring (the left column in fig. 2) and in the central region when the anchoring is normal (the right column). Either picture coincides with its counterpart when flipped over.

The shapes for both cases, shown in fig. 3, are quite dissimilar. As the material shrinks along the lines in the upper row of fig. 2 drawn along the director orientation while extending normally to these lines, the ellipse becomes more slender in the case of normal anchoring and fattens when the anchoring is tangential. The shapes strongly depend on the parameters of the problem — bending rigidity κ and the metric factor a . For example, the number of folds decreases with growing κ , as seen by comparing figs. 3(a,b). Figure 4 shows the dependence on the metric factor a of the mean squared deviation of the surface from the original position and of the energy gain in a deformed elliptic domain, compared with a stressed flat sheet.

3.3 Two-hole domains

Negatively charged defects appear when domains are not simply connected. Inserting a single hole with the same anchoring as on the outer boundary leads to a lowest-energy texture with no defects. When a second hole is added, two defects with the charge $-1/2$ must appear. The position of defects depends on the size and position

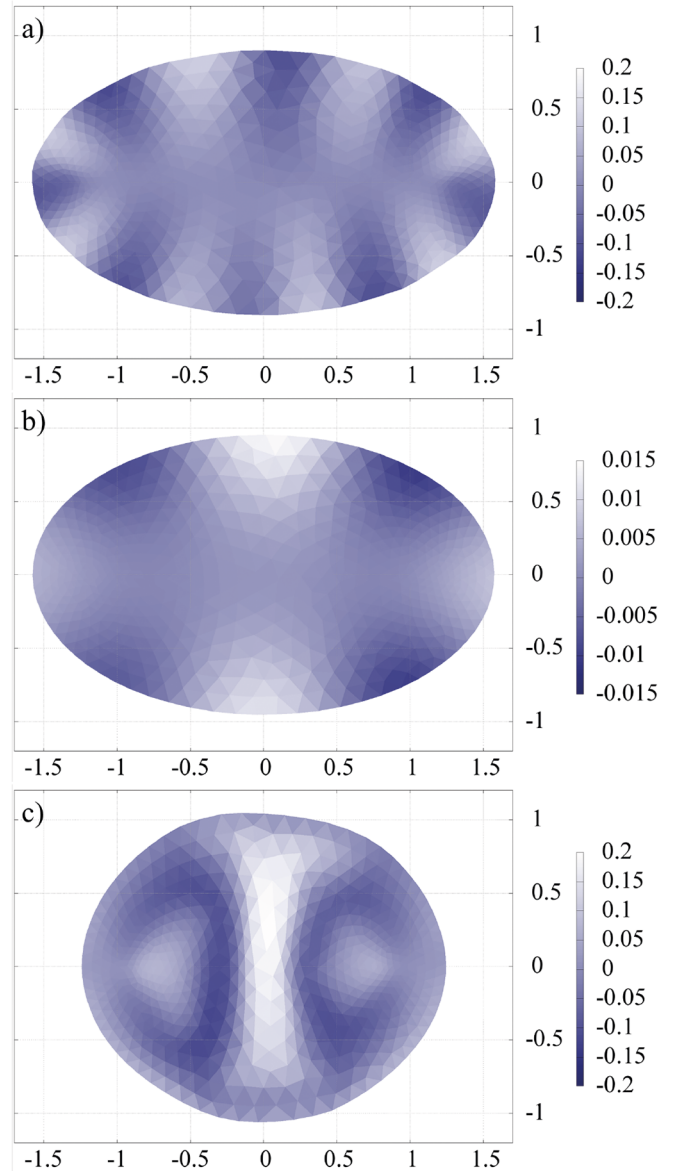


Fig. 3. Shade-coded relief maps of 3D shapes obtained for elliptic domains with normal (a,b) and tangential (c) boundary anchoring at $a = 0.1$, $\kappa = 5 \times 10^{-6}$ (a,c), and $\kappa = 10^{-4}$ (b).

of holes. Some typical examples of elliptic domains with symmetrically placed two holes, as they deform following NIT, are shown in figs. 5, 6. In all cases, the anchoring at all boundaries is normal. The corrugated shapes obtained following NIT, are, naturally, different in all cases.

In fig. 5 where the holes are relatively small, the defects are situated symmetrically on the line connecting the centres of both holes. The detailed shape near defects, that should be similar to that in the right column of fig. 1, is not resolved on the scale of relief maps in this and the following figure. It is better seen in the high-resolution relief map of Gaussian curvature in the lower panel of fig. 5.

In the upper panel of fig. 6, where the holes are large, the defects are placed on the symmetry axis separating the holes. The arrangement of defects in the two lower panels

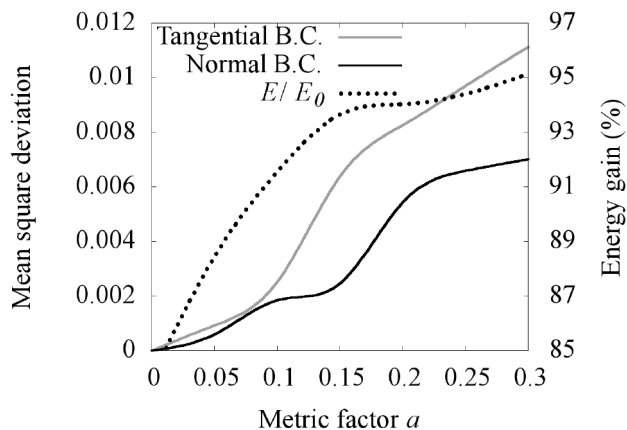


Fig. 4. The mean square deviation of the surface from the original plane (solid lines) and the energy gain in a deformed elliptic domain compared to a flat stressed elliptic sheet with tangential anchoring (dotted line) plotted against the metric factor a .

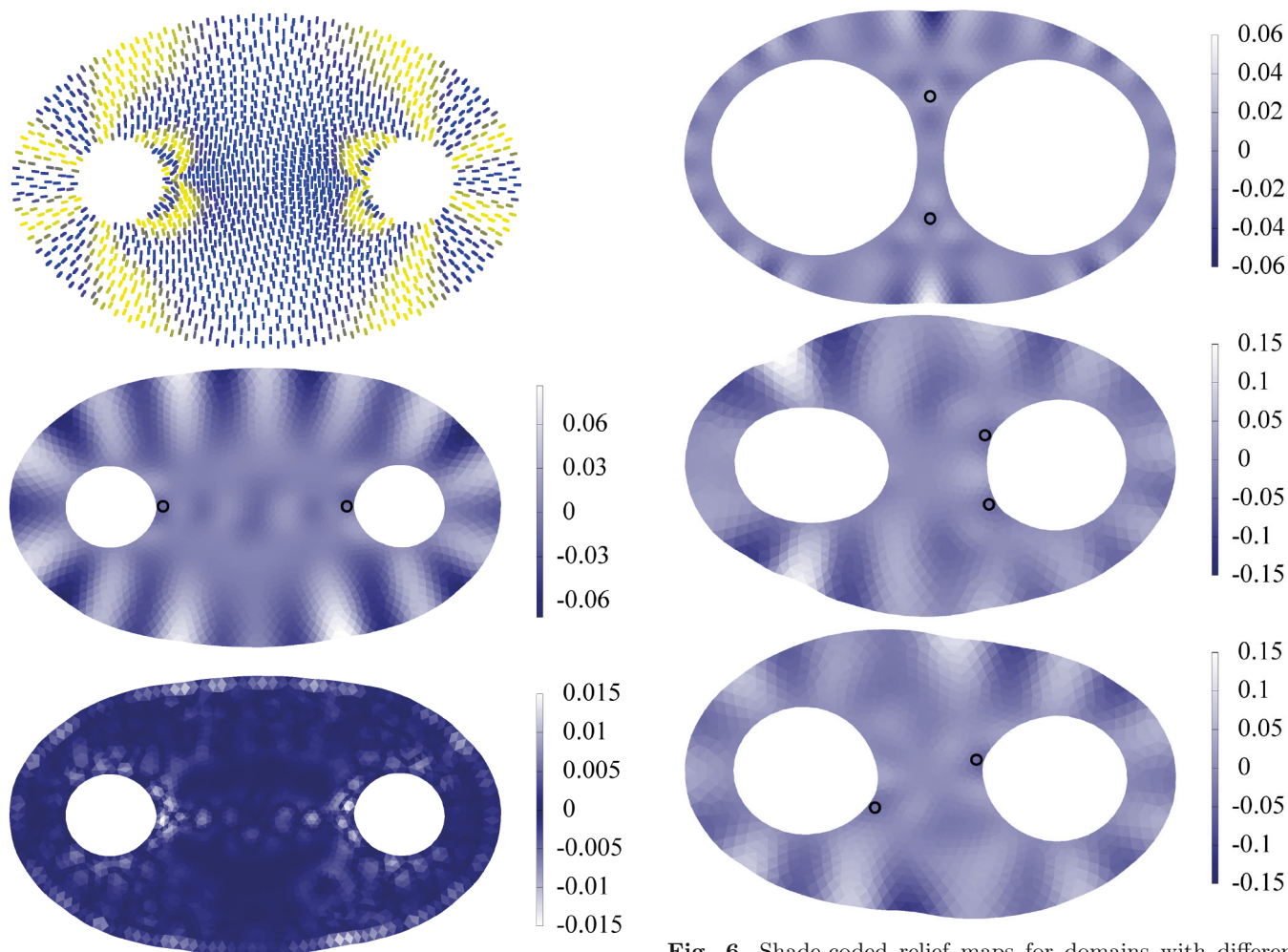


Fig. 5. Domains with two holes and defects with the charge $-1/2$. Above: the director field shaded in a way imitating the view in cross-polarisers. Middle panel: shade-coded relief map for the same configuration ($a = 0.1$); small circles mark positions of defects. Below: high-resolution shade-coded relief map of Gaussian curvature.

Fig. 6. Shade-coded relief maps for domains with different hole sizes ($a = 0.1$). Small circles mark positions of defects.

of fig. 6 with holes of intermediate size is less intuitive. In the middle panel, the defects are situated asymmetrically near one hole, while in the lower panel they are placed diagonally near alternative holes keeping a larger mutual separation. The latter arrangement has a lower energy, so that its counterpart is *metastable*.

4 Conclusion

Reshaping of nemato-elastic sheets or shells opens ways of creating a variety of forms that can be manipulated by boundary anchoring, positioning of defects, and topological changes. Besides static reshaping, the forms can be actuated dynamically, thereby creating crawling and swimming micro robots that will be the subject of a further study.

Author contribution statement

Both authors contributed equally to the paper.

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